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Novel crack-width visual measurement based on backbone double-scale features for improved detection automation

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Abstract:	<p>State-of-the-art machine-vision systems have limitations associated with crack width measurements. The sample points used to describe the crack width are often subjectively defined by experimenters, which obscures the crack width ground truth. Consequently, in most related studies, the uncontrollable system errors of vision modules result in unsatisfactory measurement accuracy. In this study, the cracks of a reservoir dam are taken as objects, and a new crack backbone refinement algorithm and width-measurement scheme are proposed. The algorithm simplifies the redundant data in the crack image and improves the efficiency of crack-shape estimation. Further, an effective definition of crack width is proposed that combines the macroscale and microscale characteristics of the backbone to obtain accurate and objective sample points for width description. Compared with classic methods, the average simplification rate of the crack backbone and the average error rate of direction judgment are all improved. The results of a series of experiments validate the efficacy of the proposed method by showing that it can improve detection automation and has potential engineering application.</p>
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The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Highlights

- Backbone neighborhood distribution points are reduced to facilitate classification.
- Dual-scale backbone features are combined for accurate width measurement direction.
- A detailed visual measurement process of crack width is proposed, providing stable and continuous measurement.
- A visual measurement method of crack width that is closer to reality is used to obtain more accurate results.
- Two evaluation standards of measurement (i.e., recall rate and direction error) are added to enable a more comprehensive evaluation of the measurement method.

1 Novel visual crack width measurement based on backbone double-scale features for 2 improved detection automation

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16 **Abstract:** State-of-the-art machine-vision systems have limitations associated with crack width
17 measurements. **The sample points used to describe the crack width are often subjectively defined**
18 **by experimenters, which obscures the crack width ground truth.** Consequently, in most related
19 studies, the uncontrollable system errors of vision modules result in unsatisfactory measurement
20 accuracy. In this study, the cracks of a reservoir dam are taken as objects, and a new crack
21 backbone refinement algorithm and width-measurement scheme are proposed. The algorithm
22 simplifies the redundant data in the crack image and improves the efficiency of crack-shape
23 estimation. Further, an effective definition of crack width is proposed that combines the
24 macroscale and microscale characteristics of the backbone to obtain accurate and objective sample
25 points for width description. Compared with classic methods, the average simplification rate of the
26 crack backbone and the average error rate of direction determination are all improved. The results
27 of a series of experiments validate the efficacy of the proposed method by showing that it can
28 improve detection automation and has potential engineering application.

29
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31 1 Introduction

32 Cracks are a common type of structural damage that jeopardize the health of concrete
33 buildings (e.g., roads, bridges, tunnels, and dams) [1–5]. Regular inspections and repairs can
34 reduce the risk of structural collapse during natural disasters (e.g., earthquakes and floods) [6–10].

1 35 Researchers have proposed a variety of innovative methods to replace traditional manual visual
2 36 inspection [11–14]. However, their methods target larger, more complex field-environment crack
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4 37 detection tasks that are expensive, slow and susceptible to external interference [15–18] .
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6 38 Non-contact, high-precision computer-assisted visual measurement has shown good performance
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8 39 in various inspection fields [19–23] and is a promising method to replace human visual
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10 40 inspections. Researchers have provided a relatively complete process framework for mapping
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12 41 image pixel features to geometric dimensions in real physical space [24,25] . However, for
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14 42 complex slender and irregular targets, such as cracks, the current measurement applications lack
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16 43 geometric meaning, and their accuracy is not sufficient [26].

18 44 Regarding the identification and segmentation of cracks, researchers have applied the classic
19
20 45 digital image processing (DIP) method and neural-network models to make the extraction of
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22 46 cracks more robust [27–32]. Kim et al. [33] compared the threshold segmentation effects of five
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24 47 classic threshold segmentation algorithms on concrete cracks and showed that the less robust
25
26 48 threshold segmentation suffers background complexity, large changes in illumination, and
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28 49 inconsistencies. **It is generally difficult to accurately detect cracks under uniform conditions.** Other
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30 50 researchers have proposed semantic segmentation models that have been effective in solving these
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32 51 problems [34–37]. Many scholars have also proposed corresponding model structures specifically
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34 52 for crack detection. For example, Zou et al. developed the DeepCrack [27] network based on
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36 53 SegNet and achieved an F-measure greater than 0.87. They improved the segmentation accuracy
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38 54 but introduced larger scale parameters. Ju et al. developed the CrackU-net [38] model, which
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40 55 improved on U-Net and FCN and achieved an accuracy of 99.01%. Wang and Cheng combined
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42 56 DilaSeg and RNN and proposed DilaSeg-CRF [29] for segmentation cracks, which achieved a
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44 57 20% to 32% improvement compared to the classic semantic segmentation model. Zhang et al.
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46 58 designed CrackNet [39] without a pooling layer in an attempt to reduce the accuracy loss in the
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48 59 crack segmentation process. Then, they combined it with an RNN and proposed CrackNet-R [28]
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50 60 to improve the accuracy of segmentation, subsequently obtaining a higher recall rate and
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52 61 F-measure. These neural-network methods were optimized for concrete cracks and provided more
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54 62 opportunities for improvement. However, increasing the network depth to improve accuracy

63 increases the burden on the hardware in the application process.

64 The quantitative analysis of crack-hazard degree (e.g., crack length, width, and depth) is
65 presently insufficient [17,40] . For example, clearly defining a crack width from a visual
66 measurement and continuously performing such measurements remain quite challenging
67 [26,41,42]. Historically, researchers used an edge or a skeleton of the crack as the basis for width
68 measurement [43], but several problems remain. For example, the two edges of a crack may be
69 quite different in the local area, and it is difficult to obtain accurate measurement directions. The
70 crack skeletons obtained by improved refinement algorithms must still handle redundant data, and
71 the definition of the skeleton remains inaccurate.

72 Researchers have attempted to use these features to define the crack-width visual
73 measurement method and achieved varying results. For example, Asjod et al. [44] proposed the
74 arc-length method to measure cracks. Further, Wang et al. [26] proposed a Laplace-based
75 continuous explicit measurement method that simulates the crack as an electric field in a capacitor,
76 and used the total length of the trajectory of electrons in the cathode and anode of a capacitor to
77 define the width of the crack. However, the width obtained by their method is the length of a curve,
78 not a straight-line distance needed for engineering. Kim et al. [45] proposed using the two edge
79 points closest to the crack skeleton point for width measurement. Luo et al. [46] investigated the
80 crack edges from the crack skeleton point in four directions and took the minimum distance
81 between the two edges in the four directions as the width of the crack. Their method performs well
82 with idealized cracks. However, in reality, the width often refers to the straight-line distance
83 between the two edges in the normal direction of the crack-growth direction, and the crack edges
84 often have irregular bumps. Hence, the two edges are not strictly symmetrical about the skeleton.

85 The above methods use measurement points that do not match the geometric meaning of
86 width. Therefore, the measurement correctness must be improved. The comprehensiveness of
87 using only numerical results as the evaluation criteria of measurement methods needs to be
88 improved. In addition, whereas many studies have focused on road cracks, only a few have
89 focused on dam cracks, which have characteristics of large image noise, complex background
90 texture, and random location [47,48] . The research object needs to be expanded, thus, a large

1 91 scope exists for machine-vision measurement research in this area.

2 92 In this study, we selected a reservoir dam crack located in the field as the research object and
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4 93 developed a more streamlined crack backbone extraction algorithm, based on an improved
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6 94 image-refinement algorithm, that enhances the backbone's ability to describe crack shapes. Further,
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8 95 we devised a more accurate measurement direction by combining the backbone macroscale slope
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10 96 characteristics and microscale neighborhood distribution characteristics. Then, defining the width
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12 97 of the crack as the straight-line distance between two measurement points located at the edge of
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14 98 the crack in the measurement direction, we developed a crack-width measurement method. Two
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16 99 evaluation criteria are included: the measurement recall rate and direction error. Compared with
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18 100 the method proposed by Luo et al. [46], the method proposed here is more comprehensive, in that
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20 101 it has a more accurate visual measurement performance that aligns with the geometric meaning of
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22 102 width. This study makes the following contributions:

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25 103 1. A detailed visual crack width measurement process is proposed that can provide stable and
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27 104 continuous measurements.

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29 105 2. Based on the improved image-refinement algorithm used to further refine the complete
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31 106 crack backbone, the neighborhood distribution types of backbone points are reduced to facilitate
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33 107 their use in classifying backbone points.

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35 108 3. Combining the macro and micro characteristics of the backbone, a visual crack width
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37 109 measurement method that is closer to the actual needs of the project is used to obtain a more
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39 110 accurate measurement method.

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41 111 4. Two evaluation measurement standards (i.e., recall rate and direction error) are added to
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43 112 enable a more comprehensive evaluation of the measurement method.

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45 113 The remainder of this article is structured as follows. The process and principle of the crack
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47 114 width measurement method are described in Section 2. Section 3 presents the relevant evaluation
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49 115 test conducted on the proposed method. Section 4 provides concluding remarks and outlines
50
51 116 possible future study.

52
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54
55 117 **2 Methods**

118 2.1 Visual crack-measurement process

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3 119 The basic processes of the width-measurement method proposed in this study include crack
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5 120 segmentation, backbone refining, and width measurement. The specific process is shown in Fig. 1.
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7 121 Previous studies have shown that the U-Net semantic segmentation model is sensitive to edge
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9 122 detail features, which also suggests that it would be suitable for dam-crack segmentation [49–52].
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11 123 In this article, the input into U-Net was an RGB image and the output is a semantically segmented
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13 124 binary image. The process of semantic segmentation takes place in a code-decoded symmetrical
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15 125 U-shaped structural model, hence the name U-Net. The acquisition of the parameters in the
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17 126 U-shaped structural model requires convolutional inference of a large number of labeled samples,
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19 127 the result of which is then recorded in the model file. When using U-Net, this model file is called
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21 128 and the image data is passed into the model. The segmentation result can be obtained after
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23 129 calculation by U-Net, which is a very simple and commonly used semantic segmentation model.
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25 130 In this study, the results of the U-Net semantic segmentation model were therefore directly used as
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27 131 the input material for the pretreatment of the crack backbone extraction and crack width
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29 132 measurement. Pretreatment can effectively handle possible misjudgment problems in crack
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31 133 segmentation while improving the robustness of backbone refining. Morphology (large) represents
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33 134 the morphological processing of the large window, which is used for the segmentation of the crack
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35 135 area; morphology (small) represents small window morphology processing, which is used to
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37 136 strengthen the connectivity of the crack binary image. Morphological processing here refers to
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39 137 dilation or erosion algorithms (they have opposite effects to each other), whose role is to expand
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41 138 the binarized target towards the background. Combinatorial binarization is the combined operation
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43 139 of binarization–blur–binarization, which is used to smooth the crack binary image and eliminate
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45 140 segmentation impurities before backbone extraction. The role of blur is also to expand the target,
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47 141 but its effect is more moderate than that of morphological processing.
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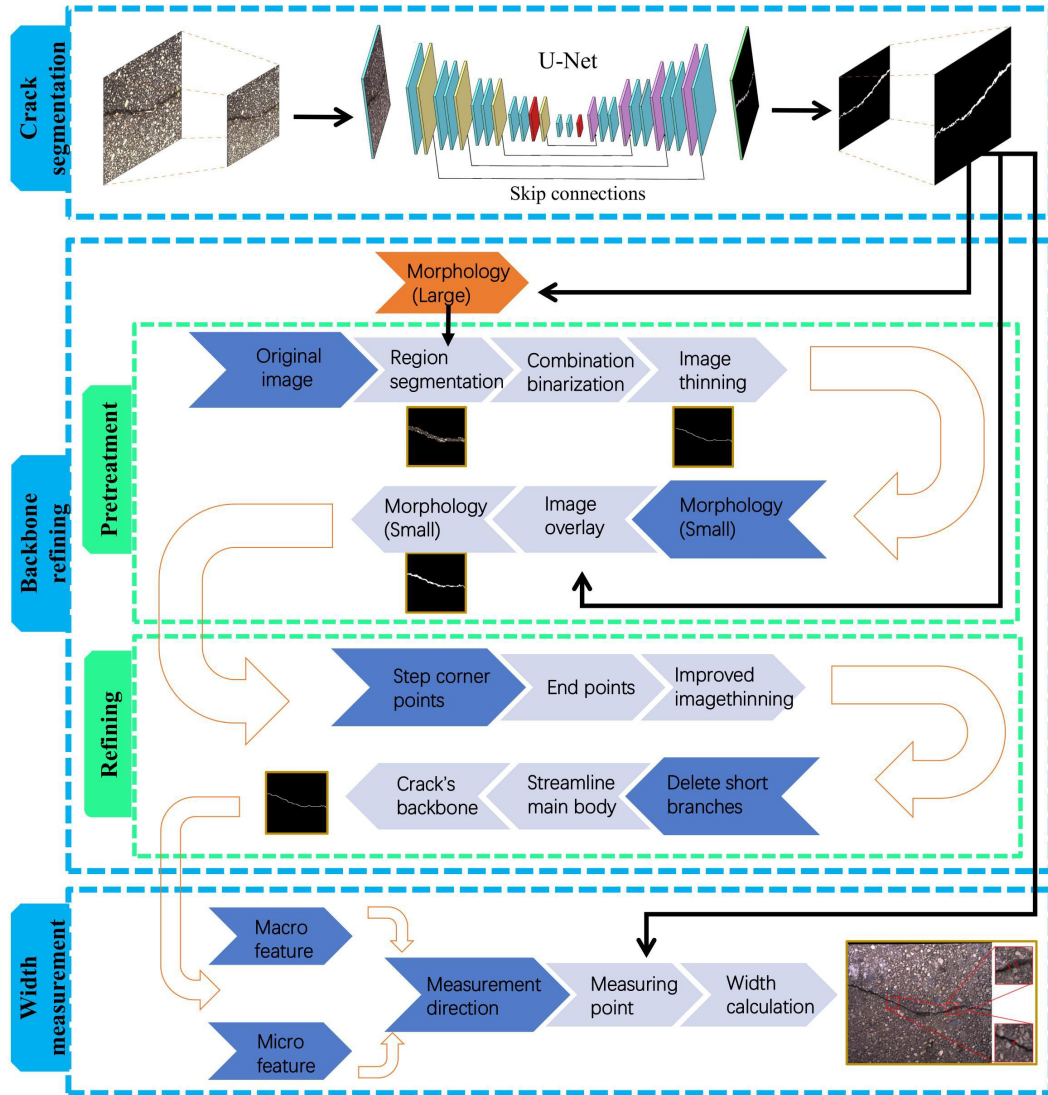


Fig. 1 Framework and flowchart for visual measurement

2.2 Crack backbone refinement

To address the problem of redundant data points when the image-refinement algorithm extracts the crack skeleton, we refine the crack skeleton and the backbone of the crack using the improved image-refinement algorithm to mark the ends of the cracks while avoiding end-shortening during refinement. The refinement of the crack backbone removes redundant points on the branches and backbones based on the skeleton.

The backbone of the crack contains information on the shape of the crack, which has the

152 function of determining its position and providing the basis for measuring its width. The classic
 153 Zhang-Suen image thinning algorithm [53] can be used to extract the crack skeleton, but the
 154 skeleton still has redundant data, which can be further streamlined to obtain the backbone of the
 155 crack. For the convenience of comparison and explanation in this work, it is stipulated that the
 156 output of the Zhang-Suen image thinning algorithm is called “skeleton”, and the output proposed
 157 for improvement and further processing based on the Zhang-Suen image thinning algorithm is
 158 called “backbone”.

159 The input into the crack backbone refinement algorithm is a crack binary image with only
 160 crack and background pixels. This process involves iterative refinement. In each iteration, the
 161 outermost contour is transformed into the background. The algorithm sets a certain crack pixel as
 162 P_0 . Starting from the pixel just above P_0 , the eight neighborhoods of P_0 are set as P_1 to
 163 P_8 , clockwise. The background point is assigned a value of either zero or one, as shown in Fig.
 164 2.

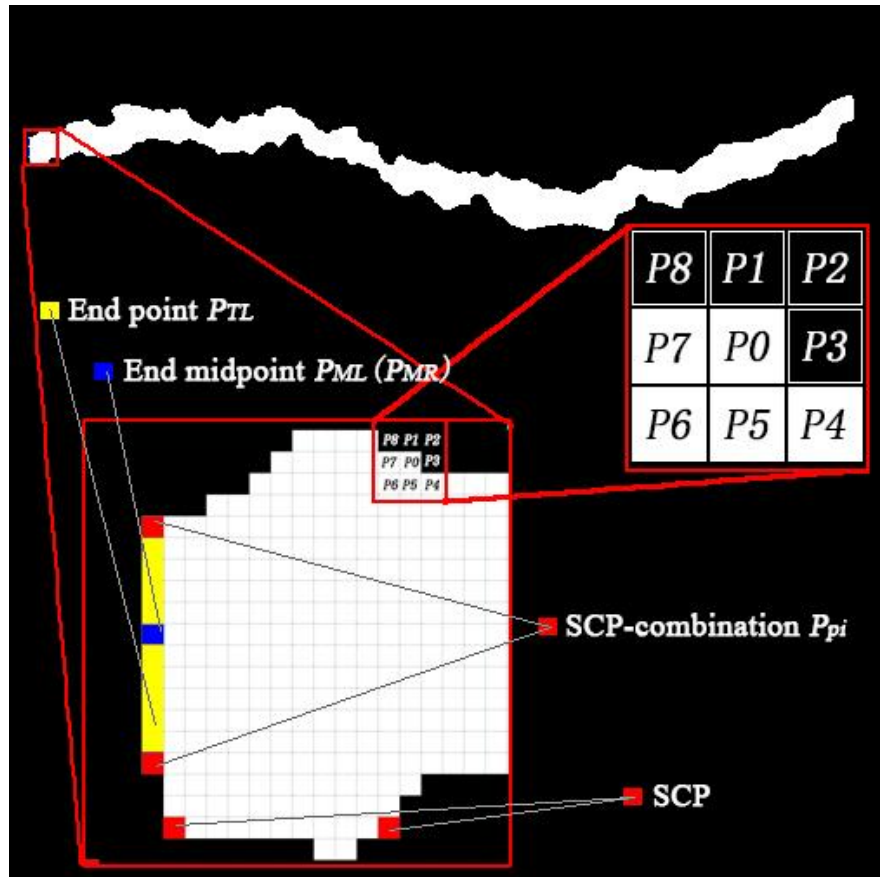


Fig. 2 Feature points in crack binary graph

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168 Detecting the edge of the crack binary image involves multiple steps. As shown in Fig. 2,
169 each step with a vertex height greater than 1 pixel is the step corner point (SCP), which can be
170 found according to its eight-neighborhood features and is used to build set CoP . Let $P_0(\Delta P)$
171 denote the set of P_0 's eight neighborhoods satisfying condition ΔP . The set, CoP , is given by
172 the formula $CoP = \{P_0 | P_0(\Delta P)\}$, in which ΔP is defined by Eq. (1):

$$\begin{aligned} & \exists(P_1 + P_2 + P_3 = 3 \wedge P_5 + P_6 + P_7 + P_8 = 0) \\ & \vee(P_3 + P_4 + P_5 = 3 \wedge P_1 + P_6 + P_7 + P_8 = 0) \\ & \vee(P_5 + P_6 + P_7 = 3 \wedge P_1 + P_2 + P_3 + P_4 = 0) \\ & \vee(P_7 + P_8 + P_1 = 3 \wedge P_2 + P_3 + P_4 + P_5 = 0), \quad P_0 \in P_0(\Delta P) \end{aligned} \quad (1)$$

174 In CoP , the two SCPs in the same column are recorded as a set, P_{pi} , and its midpoint,
175 P_{piM} , is marked from there, as shown in Fig. 2. Then, according to the eight-neighborhood
176 feature, the P_{piM} in the left and right ends of the crack, which are regarded as P_{ML} and P_{MR} ,
177 can be separated from the set of all P_{piM} . P_{ML} and P_{MR} 's eight neighborhoods at the left and
178 right ends to satisfy Eq. (2).

$$\begin{aligned} & (a) P_6 + P_7 + P_8 = 0 \Rightarrow P_{ML} \\ & (b) P_2 + P_3 + P_4 = 0 \Rightarrow P_{MR} \end{aligned} \quad (2)$$

180 The pixels in the same column as P_{ML} or P_{MR} are the crack's end points—recorded as P_{TL}
181 and P_{TR} , respectively. If P_{TL} and P_{TR} 's eight neighborhoods satisfy the condition $P_1 + P_5 = 2$,
182 they are respectively recorded in sets $TePL$ and $TePR$. The purpose of this move is to eliminate
183 the points overlapping the edges among the endpoints during the refinement process.

184 Let $A(P_0)$ denote the number of 01 patterns of the clockwise connections in the eight
185 neighborhoods of P_0 and $B(P_0)$ denote the number of crack pixels in the eight neighborhoods
186 of P_0 . One iteration of the crack backbone extraction algorithm is divided into odd- and
187 even-numbered sub-iterations. In each sub-iteration, the crack pixels that satisfy Eq. (3) are

188 marked as the outermost pixels, which are uniformly converted into background pixels before the
 189 iteration completes. In even-numbered sub-iterations, only conditions (c), (d), and (e) are
 190 respectively changed to (c'), (d'), and (e').

$$\begin{aligned}
 & (a) A(P_0) = 1 \\
 & (b) 2 \leq B(P_0) \leq 6 \\
 & (c) P_1 \times P_3 \times P_5 = 0 \\
 & (d) P_3 \times P_5 \times P_7 = 0 \\
 & (e) P_0 \notin TePR \\
 & (c') P_1 \times P_3 \times P_7 = 0 \\
 & (d') P_1 \times P_5 \times P_7 = 0 \\
 & (e') P_0 \notin TePL
 \end{aligned} \tag{3}$$

192 The algorithm iteratively thins the cracks to obtain the skeleton according to the above rules
 193 until no crack pixels are marked as outermost pixels. However, there are still numerous redundant
 194 points in the skeleton that can be streamlined further. The streamlining process is divided into two
 195 steps: deleting short branches and streamlining the skeleton's main body to obtain the backbone.

196 To delete short branches, the skeleton's endpoints are marked on the left and right sides of the
 197 image and other endpoints satisfying $B(P_0) < 2$, or $B(P_0) = 2$ and $A(P_0) = 1$, apart from the
 198 skeleton's endpoints. Once an end point is deleted on the short branch, the connected point
 199 becomes the new endpoint. These operations are repeated several times until all short branches are
 200 deleted. The deletion process is illustrated in Fig. 3.

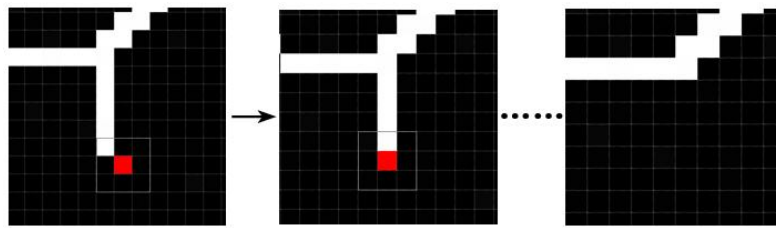


Fig. 3 Short branch deletion process

203 The refinement of the backbone is to convert pixels in the skeleton line that satisfy any of the
 204 items in Eq.(4) to the background. If the image is scanned from the first pixel in the upper left
 205 corner to the last pixel in the lower right corner, then, as shown in Fig. 4, the red pixels are deleted.

206 **After cleaning, the backbone is obtained with the following features:**

207 (1) The total number of backbone pixels in each point's eight-neighborhood does not exceed

208 2.

209 (2) Its eight-neighborhood pixel distribution will show four shapes: v shape, linear shape,

210 semi-Y shape of left and semi-Y shape of right. Plus, when each shape is rotated around the center,

211 the number of neighborhood distribution types of backbone points is reduced to

212 $C_4^2 + C_2^1 + C_4^1 C_2^1 = 16$, as shown in the lower right corner of Fig. 4.

213

$$\begin{aligned} (a) P_1 + P_3 &= 2 \\ (b) P_1 + P_7 &= 2 \\ (c) P_5 + P_3 &= 2 \\ (d) P_5 + P_7 &= 2 \end{aligned} \quad (4)$$

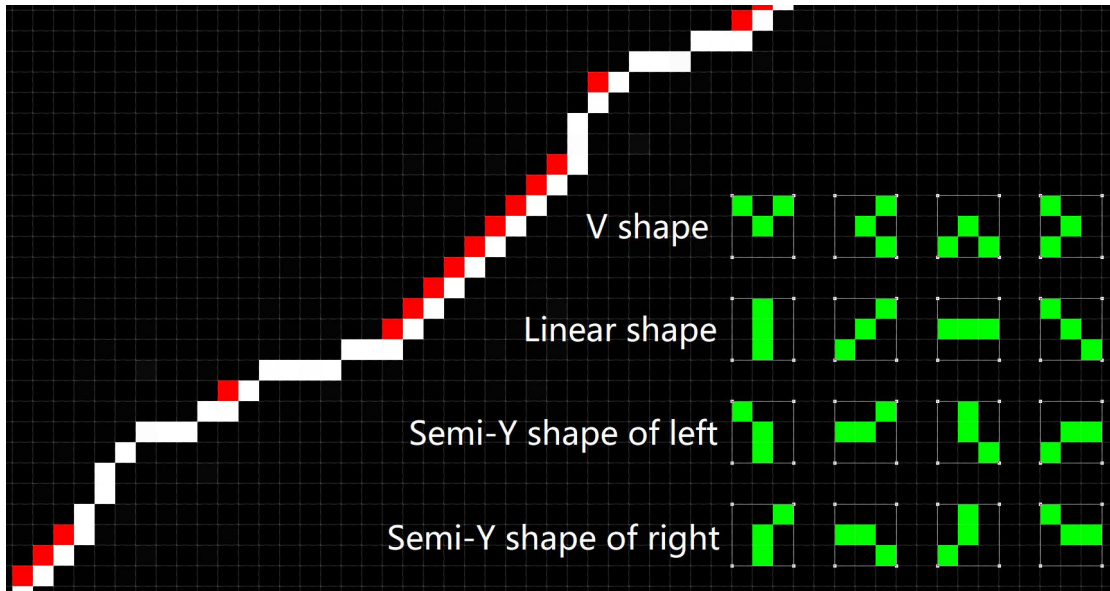


Fig. 4 Streamlined backbone

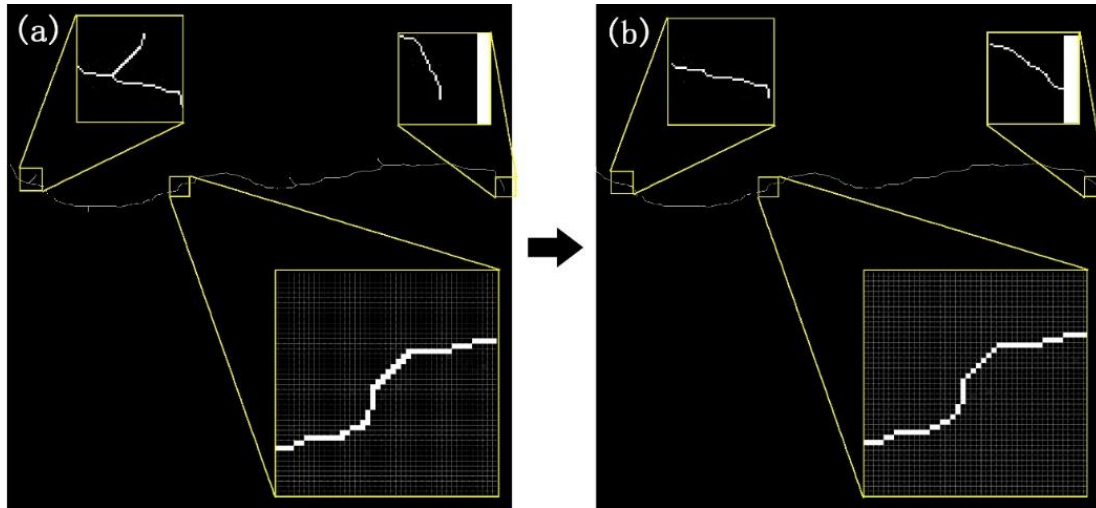
216 Fig. 5 illustrates the effect of the main crack extraction. The backbone extraction algorithm in
217 this paper is more streamlined than others. In total, compared with the classic Zhang-Suen image
218 thinning algorithm, the crack backbone refinement algorithm in this paper has the following
219 characteristics:

220 1. The branches are removed and the shape of the end of the crack is retained (as shown in
221 the upper left corner of Fig. 5a and upper right corner of Fig. 5b);

222 2. The eight-neighborhood effective pixels of the backbone do not exceed 2 and there are

223 only 16 types of neighborhood pixel distribution (as shown in the lower right corner of Fig. 4 and
224 the lower right corner of Fig. 5).

225 While simplifying the amount of data, it is convenient to use the neighborhood distribution
226 type to classify the backbone points, which is conducive to the subsequent clear definition of the
227 crack-width measurement.



228
229 Fig. 5 Classic thinning algorithm (a) compared with the improved backbone refining
230 algorithm in this study (b)
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232 2.3 Determining the crack width measurement direction

233 As shown in Fig. 6, there are multiple measurement schemes that rely on the same
234 measurement position, O. The measurement schemes AE, BF, CG and DH are the
235 width-measurement results obtained at position O in different measurement directions. Notably,
236 they are quite different from each other. The width is measured along the normal direction of the
237 crack-growth direction according to the visual inspection method commonly used by engineers in
238 practice. Evidently, the solution BF is more suitable for characterizing the width of the crack at
239 position O. The main objective of this section is to get as many measurement points as possible
240 and determine the width of the crack in the visual measurement along the optimum measurement
241 direction to closely approximate the width obtained by the commonly used method in practice.

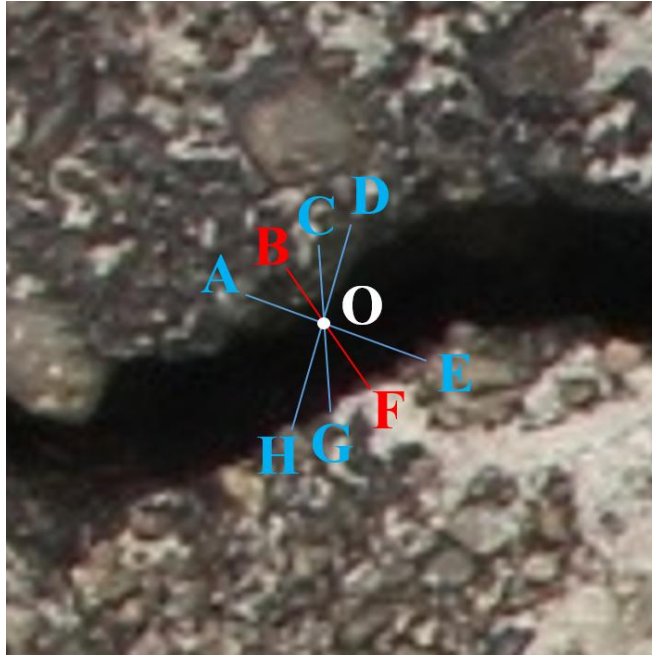


Fig. 6 Different measurement methods on the same crack

This paper proposes a method for determining the direction of crack width measurement based on the dual-scale features of the backbone. The proposed method combines the slope information of the crack backbone at the macroscale with its neighborhood information at the microscale. The macroscale information is based on the trend of the entire backbone of the crack, whereas the microscale information is based on the neighborhood distribution information of each pixel of the crack backbone. The combined method defines eight measurement directions, and then macro- and micro-scale information is matched to each of these eight directions. When the dual-scale information matches, the measurement direction can be determined and obtained. For points where the macroscale and microscale information do not match, the measurement is abandoned. Because the point where the direction is incorrect or cannot be measured will affect the reliability of the measurement result.

At the macro level, this study uses the least-squares method to fit the n-degree polynomial curve of the main stem into a polynomial function, $v = f(u)$, as established in Eq. (5):

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$$\begin{aligned}
 \begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_m \end{bmatrix} &= \begin{bmatrix} 1 & u_1 & \cdots & u_1^n \\ 1 & u_2 & \cdots & u_2^n \\ \vdots & \vdots & \ddots & \vdots \\ 1 & u_m & \cdots & u_m^n \end{bmatrix} \times \begin{bmatrix} w_1 \\ w_2 \\ \vdots \\ w_n \end{bmatrix} \\
 \mathbf{V} &= \mathbf{U} \times \mathbf{W}
 \end{aligned} \tag{5}$$

where (u_m, v_m) is the coordinate value of the backbone point in the image coordinate system, W is the coefficient matrix of the polynomial function, m is the number of backbone points participating in the polynomial curve-fitting, n is the order of the highest degree of the curve, and $n = 9$.

The least-squares method is used to solve matrix W , as shown in Eq. (6):

$$\mathbf{W} = (\mathbf{U}^T \mathbf{U})^{-1} \mathbf{U}^T \mathbf{V}. \tag{6}$$

The first-order derivative of the function can be used to obtain the slope, dv_m , at any point on the backbone, as shown in Eq. (7):

$$dv_m = \sum_{i=1}^n a_{n-i} u_m^{n-i-1}. \tag{7}$$

The angle, θ , between a straight line passing through any backbone point and the horizontal axis represents the measurement direction. This study defines eight measurement directions with an interval of 22.5° between each. At the macro level, mapping is defined from the slope, dv_m , of the curve, $v = f(u)$, to the macro measurement direction, ϕ , as shown in Eq. (8).

$$\phi = \begin{cases} 0^\circ, dv_m \in (-\infty, \tan 101.25^\circ) \cup [\tan 78.75^\circ, +\infty) \\ 22.5^\circ, dv_m \in [\tan 101.25^\circ, \tan 123.75^\circ) \\ 45^\circ, dv_m \in [\tan 123.75^\circ, \tan 146.25^\circ) \\ 67.5^\circ, dv_m \in [\tan 146.25^\circ, \tan 168.75^\circ) \\ 90^\circ, dv_m \in [\tan -11.25^\circ, \tan 11.25^\circ) \\ 112.5^\circ, dv_m \in [\tan 11.25^\circ, \tan 33.75^\circ) \\ 135^\circ, dv_m \in [\tan 33.75^\circ, \tan 56.25^\circ) \\ 157.5^\circ, dv_m \in [\tan 56.25^\circ, \tan 78.75^\circ) \end{cases}. \tag{8}$$

At the microscale, there are only 16 types of eight-neighborhood distributions of backbone points, and the number is relatively small. The mapping from the backbone point to the microscale

275 measurement direction, φ , can be defined according to the eight-neighbor distribution types, as
 276 shown in Eq. (9).

$$277 \quad \varphi = \begin{cases} 0^\circ, (p1 + p5 = 2) \vee (p6 + p8 = 2) \vee (p2 + p4 = 2) \\ 22.5^\circ, (p1 + p4 = 2) \vee (p5 + p8 = 2) \vee (p1 + p5 = 2) \\ 45^\circ, (p4 + p8 = 2) \vee (p1 + p4 = 2) \vee (p5 + p8 = 2) \\ 67.5^\circ, (p4 + p7 = 2) \vee (p3 + p8 = 2) \vee (p3 + p7 = 2) \\ 90^\circ, (p3 + p7 = 2) \vee (p4 + p6 = 2) \vee (p2 + p8 = 2) \\ 112.5^\circ, (p2 + p7 = 2) \vee (p3 + p6 = 2) \vee (p3 + p7 = 2) \\ 135^\circ, (p2 + p6 = 2) \vee (p1 + p6 = 2) \vee (p2 + p5 = 2) \\ 157.5^\circ, (p1 + p6 = 2) \vee (p2 + p5 = 2) \vee (p1 + p5 = 2) \end{cases} . \quad (9)$$

278 In fact, using only the macro- or micro-scale information of the backbone for direction
 279 determination may cause a large direction error. On the one hand, the polynomial curve fitted at
 280 the macroscale is continuous and smooth, and it is difficult to accurately fit the growth
 281 morphology of the crack backbone, as shown in Fig. 7; the white dots constitute the crack's
 282 backbone and the orange line is the smooth curve after fitting. They do not exactly coincide. On
 283 the other hand, at the microscale, as shown in the lower left corner of Fig. 4, only three pixels are
 284 used as the basis for direction determination at a time, which is insufficient to express the current
 285 growth state of the crack. In the blue circle in Fig. 7, manual measurement should be carried out in
 286 the 45° direction. However, as shown in the red circle, if microscale information has been used for
 287 measurements, it is measured in the vertical direction. Similarly, in the green circle, the vertical
 288 direction should be followed when taking the manual measurement. However, as shown in the
 289 yellow circle, if macroscale information has been used, it is still measured in the 45° direction.

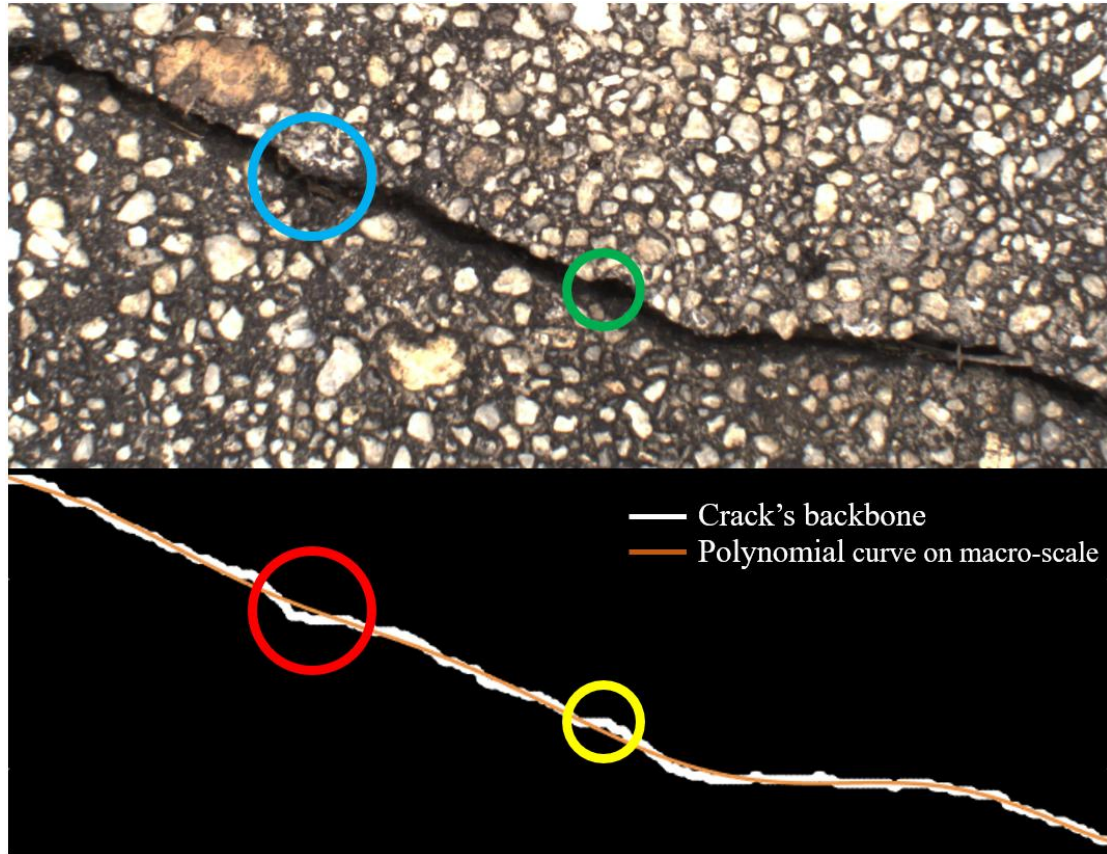


Fig. 7 Polynomial curve vs crack's backbone

Therefore, the measurement direction determination method must be designed to avoid errors in direction determination when using macroscopic or microscopic scale information alone. When solving the microscale direction, φ , this method is a situation where there are multiple neighborhood distribution types corresponding to one direction. Therefore, the microscale direction φ can be seen as a constraint on the macroscale direction, ϕ . When the macroscale, ϕ , and microscale, φ , directions of the backbone point are equal, the measurement direction, θ , of the point can be expressed as $\theta = \phi = \varphi$.

2.4 Crack width measurement

The straight line measurement, L_m , is defined according to the measurement direction and the main point, and the crack point (u, v) closest to L_m is found to form a point set, P_d , as in

Eq. (10):

$$P_d = \{(u_i, v_i) \mid |v_i - (\tan\theta * u_i + b)| < 1\}, \quad (10)$$

where b is the intercept of the linear equation, which can be obtained by substituting the coordinates of the backbone point into the equation.

The set P_d includes the upper edge measurement point, P_{mu} , and the lower edge measurement point, P_{ml} , of the crack. As shown in Fig. 8, the yellow dots indicate the crack's backbone, the red dot is the measurement position at that place, the blue dots are P_d , and the green pixels are the two measurement points found according to the above method.

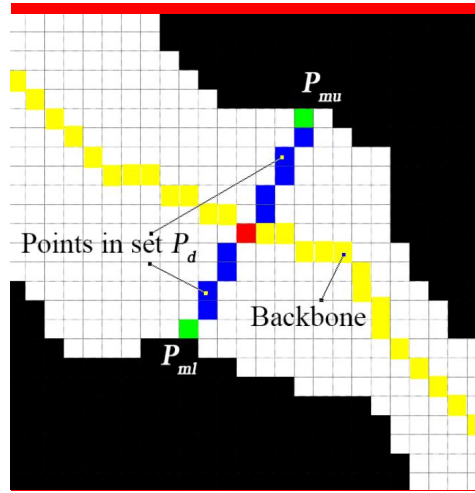


Fig. 8 Acquisition process for the measuring points

The values of P_{mu} and P_{ml} are shown in Eqs. (11) and (12):

$$P_{mu} \begin{cases} (u_{\max}, v_{\min}), 0^\circ \leq \theta < 90^\circ \\ (u_{\min}, v_{\min}), 90^\circ \leq \theta < 180^\circ \end{cases}, \quad (11)$$

$$P_{ml} \begin{cases} (u_{\min}, v_{\max}), 0^\circ \leq \theta < 90^\circ \\ (u_{\max}, v_{\max}), 90^\circ \leq \theta < 180^\circ \end{cases}. \quad (12)$$

As shown in Fig. 9, the blue line indicates the measurement method of the proposed method at this location, and the cracks covered by the blue lines can represent the range that can be measured on the crack image of this scheme.



Fig. 9 Measurable point of a section of a crack and its measurement scheme

In this study, a binocular vision system is used for width-vision measurement, and the camera's sight axis is set perpendicular to the dam surface. Before measurement, the camera must be double-targeted to correct distortion and to perform epipolar line correction between the two cameras. Template matching is used to obtain four 50×50 image blocks on the right image corresponding to the upper-left, lower-left, upper-right, and lower-right of the left image. A four-dimensional vector, $\mathbf{uB}_i = [u_{Li} \quad v_{Li} \quad u_{Li} - u_{Ri} \quad 1]^T$, is constructed for the center of each image block $(u_{Li}, v_{Li})^T$, representing the coordinates of the center point of the image block on the left image in the image coordinate system. $u_{Li} - u_{Ri}$ represents the disparity value, d , of the center point of the same image block on the left and right images. The triangulation principle, $\mathbf{CB} = \mathbf{Q} \times \mathbf{uB}$, is used to obtain the coordinates, $\mathbf{CB}_i = (X_{Ci}, Y_{Ci}, Z_{Ci}, W_i)^T$, of the centers of the four image blocks in the camera coordinate system. \mathbf{Q} is the reprojection matrix, which is obtained by the camera's dual objective setting, and W is a constant. The average of the four depth values indicates the average depth of the camera's optical center from the dam surface. Equation (13) is used to calculate the crack width, W_c , represented by the two measurement points,

$$P_{mu}(u_{mu}, v_{mu}) \text{ and } P_{md}(u_{md}, v_{md}).$$

$$W_c = \frac{\bar{Z}}{f_x \cdot f_y} \sqrt{f_y^2 \cdot (u_{mu} - u_{md})^2 + f_x^2 \cdot \pi (v_{mu} - v_{md})^2}. \quad (13)$$

338 Between these, f_x and f_y are the internal parameters of the camera, which represent the
339 product of the physical focal length of the lens and the size of each unit in the x and y directions of
340 the imaging device, respectively, which are obtained by camera calibration.

341 3 Test results and analysis

342 The test site of this study was Fenghuang Reservoir Dam in Conghua District, Guangzhou
343 City, Guangdong Province. The dam of this reservoir has obvious cracks, and the samples are
344 abundant. The test site is shown in Fig. 10.

345 For the crack backbone extraction algorithm, we set the reduction rate test to illustrate the
346 performance of the algorithm when reducing the amount of data. **To measure the performance of**
347 **the direction determination method**, we used the two evaluation criteria proposed in this study: the
348 recall rate of the direction determination and the direction error, and the corresponding judgment
349 method. A segmentation performance evaluation test and a width-vision measurement accuracy
350 test were conducted. For the ground truth, we referred to the experiment in Section 4.2 of [26].
351 Six researchers marked the cracks; the direction of the crack width was the tangent direction of the
352 commonly used crack growth, and the width was the distance between two points on the edge of
353 the crack in the measurement direction.



355
356 Fig. 10 Test equipment and environment

357 3.1 Segmentation performance evaluation

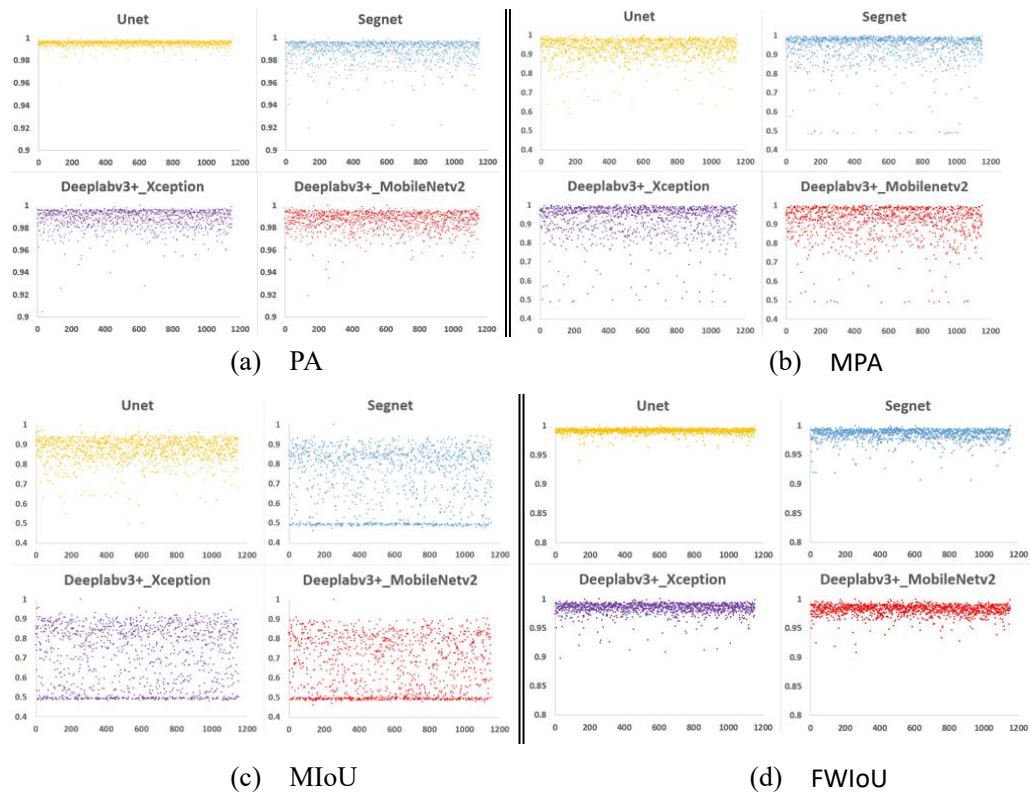
358 A total of 5,760 sample images were used for training, all samples were randomly arranged,

1 359 and the training, validation, and test sets were randomly allocated at a ratio of 6:2:2. For the
2
3 360 training input and prediction output of the model, a square image with a resolution of 400×400
4
5 361 pixels was used. The Adam optimization algorithm was used in all relevant procedures.

6 362 For the trained U-Net model, commonly used semantic segmentation evaluation indicators
7
8 363 were used (i.e., pixel accuracy [PA], average pixel accuracy [MPA], average intersection and
9
10 364 combination ratio [MioU], and frequency weight intersection and combination ratio [FWIoU]) to
11
12 365 evaluate the performance of U-Net segmentation for dam-crack evaluation. The evaluation was
13
14 366 based on a test set having 1,152 images of dam cracks. The segmentation results of the model
15
16 367 were decomposed to the original size of the test images via linear interpolation.

17
18 368 To evaluate the segmentation effect of U-Net, the crack segmentation effects of the common
19
20 369 semantic segmentation networks, SegNet and DeeplabV3+ (with Xception and MobileNetv2 as
21
22 370 the backbone networks, respectively), were added for comparison. The distributions of their
23
24 371 performance evaluation scores are shown in Fig. 11, while visual comparisons are presented in Fig.
25
26 372 12. The abscissa is the order of the graph, and the ordinate is the score.
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Fig. 11 Distribution comparison of the crack segmentation performance scores

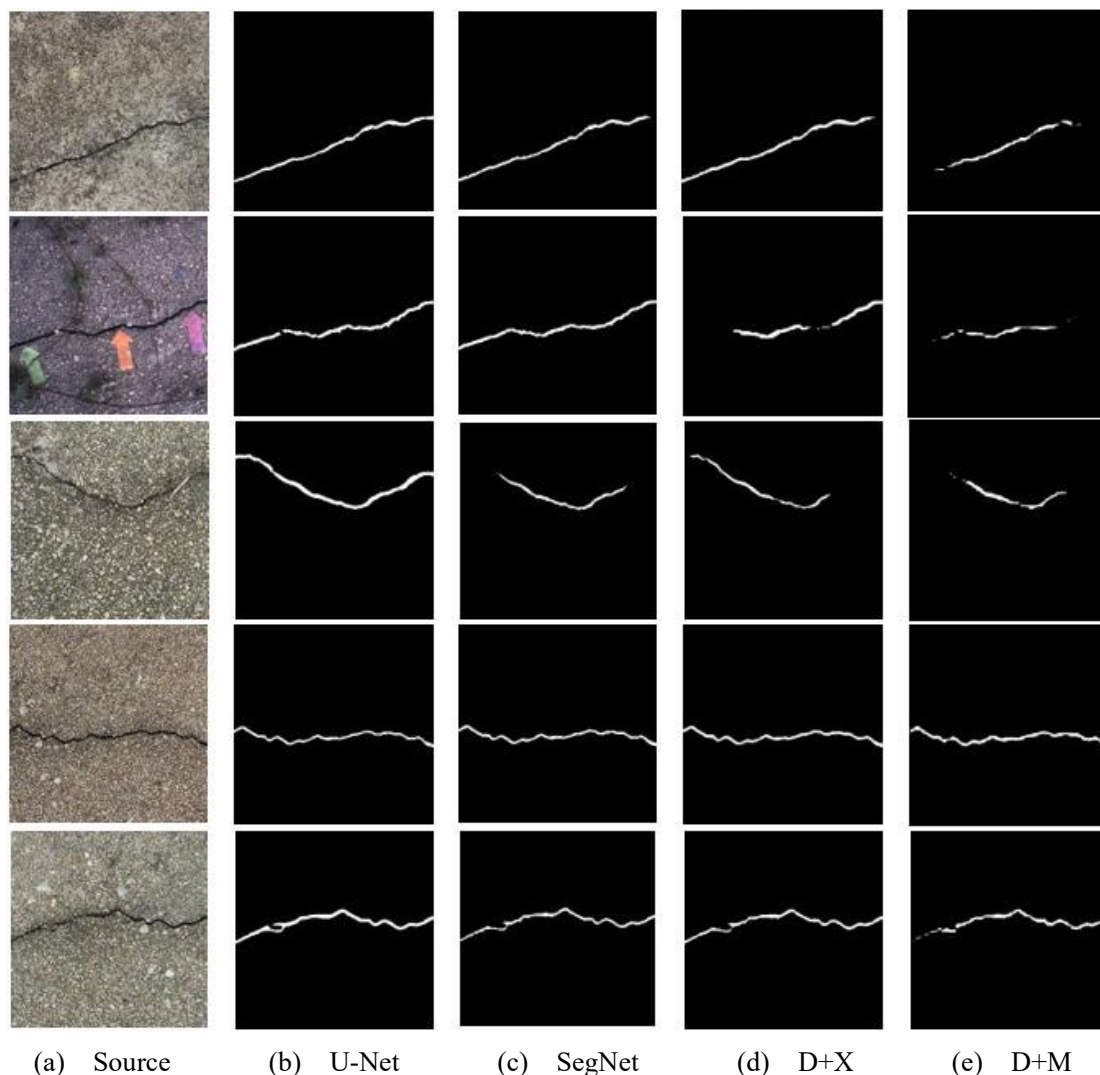


Fig. 12 Visual comparison of segmentation effects

The statistical results of the average and standard deviations of the performance evaluation scores are shown in Table 1.

Table 1. Statistics of the average and standard deviation of U-net performance evaluation scores

	PA		MPA		MIoU		FWIoU	
	Average	S.D.	Average	S.D.	Average	S.D.	Average	S.D.
U-Net	99.5 %	0.003	93.1 %	0.054	87.1 %	0.062	99.1 %	0.005
SegNet	98.9%	0.009	93.5%	0.084	72.5%	0.153	98.5%	0.010
D+X	98.8%	0.009	92.1%	0.087	70.8%	0.154	98.4%	0.011
D+M	98.6%	0.009	91.1%	0.089	65.8%	0.139	98.2%	0.010

* D+X is Deeplabv3+ with the backbone network of Xception, while D+X is MobileNetv2.

The results show that U-Net has higher segmentation accuracy and stability in the task of

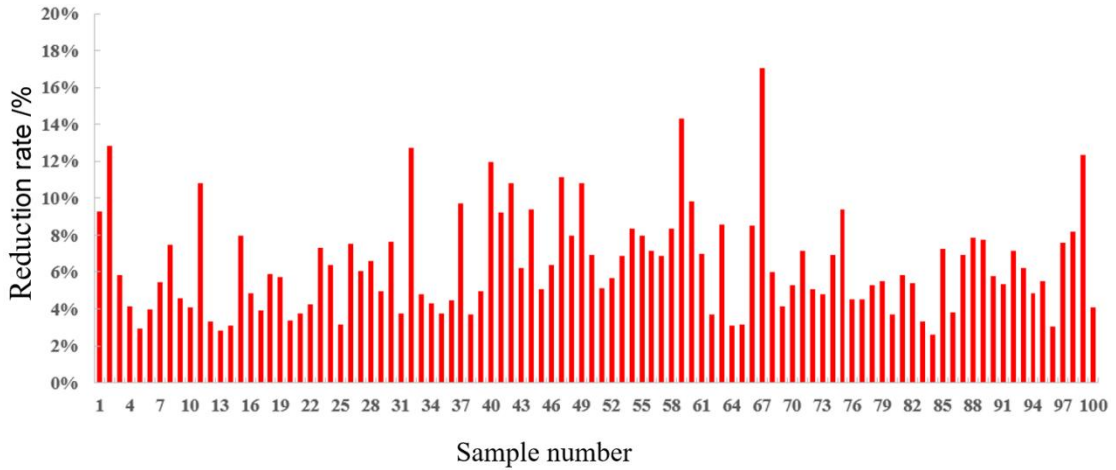
391 segmenting dam cracks than the other networks. Thus, a better improvement plan based on U-Net
 392 would be worthwhile. Consequently, U-Net segmentation results were directly used for
 393 subsequent width measurement in this study.

394 3.2 Evaluation of streamlining performance of crack backbone extraction algorithm

395 In this section, we compare the total number of backbone points (S_B , obtained by applying
 396 the backbone extraction algorithm) and the total number of skeleton points (S_S , obtained by
 397 applying the Zhang–Suen image-refinement algorithm) on the same crack segment to measure the
 398 streamlining performance of the crack backbone extraction algorithm proposed in this paper. The
 399 simplification rate of the crack backbone extraction algorithm relative to the Zhang–Suen
 400 image-refinement algorithm is R_e :

$$401 R_e = \frac{S_S - S_B}{S_S} \times 100\% . \quad (14)$$

402 Taking 100 randomly selected crack images as the samples in the experiment, the statistics of
 403 the results obtained are as shown in Fig. 13 and Table 2.



404
405 Fig. 13 Reduction rate test results

406
407 Table 2. Statistical results of the reduction rate test

	Mean	Median	Max	Min	S.D.
Reduction rate	6.40 %	5.82 %	17.04 %	2.60 %	3 %

408

1 409 As shown in Fig. 13 and Table 2, the skeleton obtained by the crack backbone extraction
2 410 algorithm had an average simplification rate of 6.40 % compared with the skeleton obtained using
3
4 411 the Zhang–Suen image-refinement algorithm. On the one hand, it showed that the skeleton
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6 412 obtained by the Zhang-Suen image thinning algorithm was universally spaced for further
7
8 413 optimization. On the other hand, the measurement direction determination method in this paper
9
10 414 was related to the eight-neighborhood pixel distribution of the backbone points, and the
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12 415 streamlining of the skeleton was conducive to the improvement of the matching degree of the
13
14 416 macro- and micro-scale measurement direction information of the backbone. Thus, the
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16 417 streamlining performance was good. In addition, it is worth emphasizing that the crack backbone
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18 418 extraction algorithm proposed in this study had no more than two neighboring points for each
19
20 419 backbone point, greatly reducing the number of backbone point neighborhood distribution types to
21
22 420 only 16, which was convenient for classifying backbone points according to neighborhood
23
24 421 distribution types.

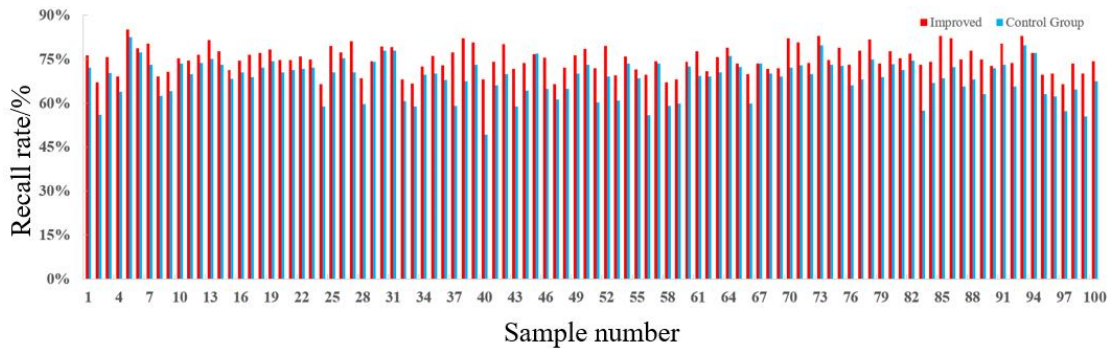
27 422 3.3 Recall rate of direction determination method

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30
31 423 The recall rate of the direction determination method refers to the ratio of the total length of
32
33 424 each segment of cracks that can be visually measured in the width to the total length of the cracks
34
35 425 in the image, which is used to investigate the recall performance of the measurement algorithm on
36
37 426 the task of crack width measurement. On the other hand, the recall rate can also reflect the
38
39 427 matching degree between the macro- and micro-scale information of the crack’s backbone in the
40
41 428 measurement direction determination problem in this method, because the backbone points of the
42
43 429 macro- and micro-scale mismatch were the negative sample in the recall statistics. Number of
44
45 430 pixels was used to approximate the length of the crack section. Using the direction determination
46
47 431 method proposed in this study, the total number of measurable points, P_c , was obtained, and the
48
49 432 total number of crack main points, P_s , was counted. The recall rate, R , is given by Eq. (15):

$$51 433 R = \frac{P_c}{P_s} \times 100\% . \quad (15)$$

52
53
54 434 In this study, 100 samples were randomly selected on the test set of U-Net crack
55
56 435 segmentation, and the segmentation results were used as samples for the recall test. In addition,

436 the control group used the same crack sample set, but the input of direction determination was the
 437 skeleton obtained by the Zhang–Suen thinning algorithm [53]. This was done to demonstrate the
 438 advantages of the proposed backbone extraction algorithm in the direction determination recall.
 439 The recall test results are shown in Fig. 14, where the red label represents the proposed method
 440 and the blue label represents the control group. The statistical results are listed in Table 3, where
 441 the label “Improved” represents the proposed method. The results show that the average recall rate
 442 of the proposed width-measurement direction determination method is approximately 74.90 %,
 443 and a standard deviation of 4 % indicated that the measurement was stable. They all outperformed
 444 the control group; the full-search performance was good overall. At the same time, the results
 445 show that the macro and micro information of the backbone points in the measurement direction
 446 determination problem were well matched, so that averaging three-quarters of the crack sections
 447 can make a more accurate measurement. More accurate here means that measurements with
 448 directions as a guide were theoretically more accurate than the measurement method which did not
 449 distinguish between measurement directions.



451 Fig. 14 Recall rate of the proposed width-measurement direction determination method

452 Table 3 Statistical results of the recall rate of the proposed direction determination method

	Mean	Median	Max	Min	S.D.
Improved	74.90%	74.73%	85.01%	66.36%	4%
Control Group	68.53%	69.82%	82.52%	49.24%	6%

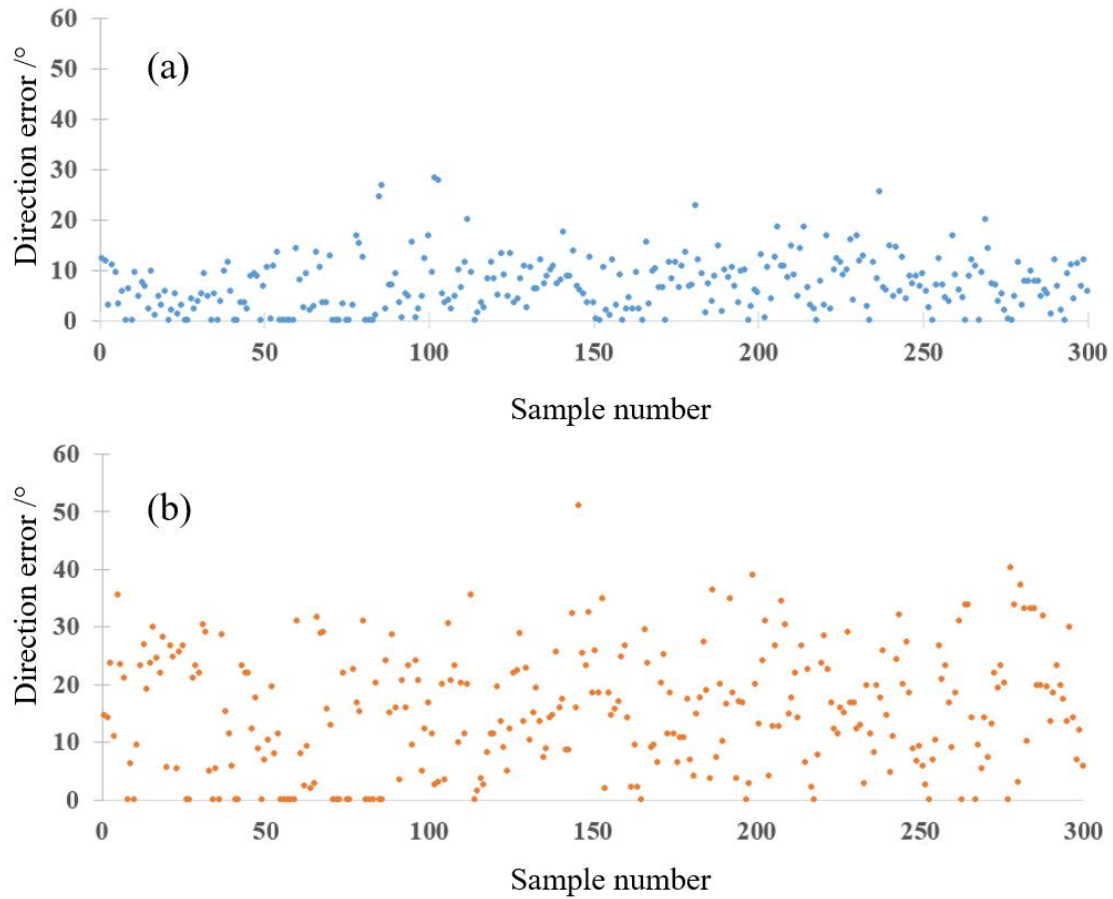
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456 **3.4 Orientation error of width measurement direction determination**

1 457 The direction error was used to evaluate the accuracy of the direction. We randomly selected
2 458 10 backbone points, P_{mi} , from the measurable points, and their positions were recorded and
3
4 459 marked on the image. We invited three technicians to determine the measurement direction of the
5
6 460 crack at the position marked on the image based on their experience, taking the tangential
7
8 461 direction of the crack-growth direction as the measurement direction. Hence, pixel points A and B
9
10 462 were selected on the two edges of the crack, and the mark point, P_m , had to be on the line
11
12 463 section AB or as close to it as possible.

14 464 The width measurement direction determination method was used to determine the
15
16 465 measurement direction of the mark point, P_{mi} , and the crack-edge points, C and D, were recorded
17
18
19 466 in this direction. We composed vectors \overrightarrow{AB} and \overrightarrow{CD} to find the acute angle between them.
20
21 467 $\Delta\theta$ represents the determination error of the measurement direction, as shown in Eq. (16).

$$24 \quad 468 \quad \Delta\theta = \arccos\left(\frac{\overrightarrow{AB} \cdot \overrightarrow{CD}}{|\overrightarrow{AB}| |\overrightarrow{CD}|}\right). \quad (16)$$

27 469 From 30 sample images, 10 points were randomly selected for testing and compared with the
28
29 470 method proposed by Luo et al. [46]. Fig. 15 shows the distribution of the test results.
30
31 471



472
473 Fig. 15. Distribution of direction errors of width measurement direction determination methods: (a)
474 proposed method; (b) method proposed by Luo et al. [46]
475

476 The statistical average, median, maximum, minimum, and standard deviation values are
477 listed in Table 4.
478

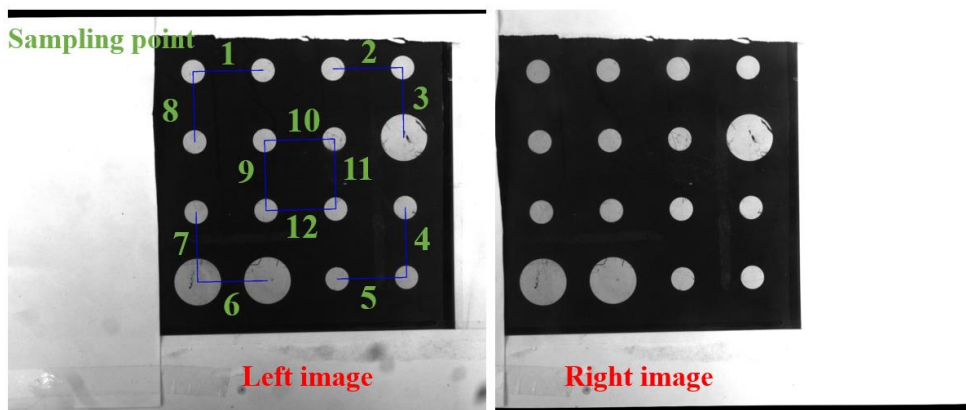
479 Table 4. Direction error statistics of width measurement direction determination methods

	Mean /°	Median /°	Max /°	Mini /°	S.D. /°
Proposed method	6.97	6.45	28.10	0	5.39
Method proposed by Luo et al.[46]	15.44	15.09	51.01	0	10.25

480
481 The direction error of the proposed direction determination method was 6.97°, the median
482 was 6.45°, the standard deviation was 5.39°, and the direction error did not exceed 28.10°, which
483 is significantly better than the method by Luo et al. [46]. The above experiments show that the
484 proposed method to determine the width measurement direction has practical accuracy and
485 stability.

486 **3.5 Test platform accuracy**

487 The spatial distance between the two corner points of the calibration board was calculated by
 488 visual measurement and compared with the actual distance, which can be used to reflect the
 489 measurement accuracy of the test platform in this study. The calibration board was placed on the
 490 dam so that both the left and right cameras could shoot all corners while maintaining the state to
 491 continuously collect 200 images of the calibration board at 2 s intervals, correct them, and select
 492 12 diagonal points on the board as sample points, as shown in Fig. 16.



494
495 Fig. 16 Left and right images of the calibration board at the test site

497 The error between the visual distance measurement and the actual distance of each sampling
 498 point was used to determine the systematic error of the test device. In the experiment, the average
 499 ($\overline{\mu_B}$) and standard deviation (σ_B) of the error data, maximum absolute error (m_B), average
 500 distance (R_B) from all repeated sampling points to the mean, and distance (D_B) between the
 501 maximum and minimum error data were used to evaluate the test device system error conditions.
 502 The results are presented in Table 5.

504 Table 5. Statistical value of the system error of the test device in this study

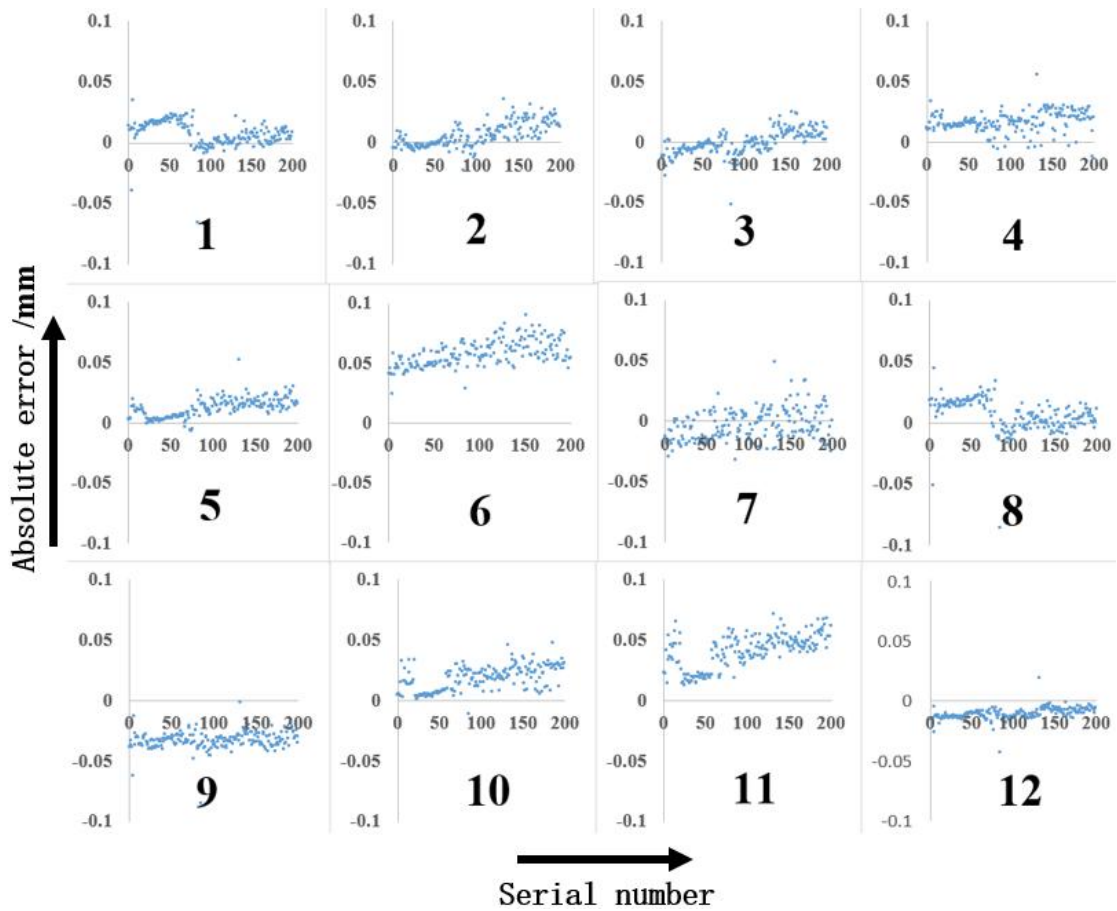
Serial number	$\overline{\mu_B}$	m_B	σ_B	R_B	D_B
Sampling point 1	0.007	0.035	0.011	-0.001	0.101
Sampling point 2	0.006	0.035	0.010	0.006	0.058
Sampling point 3	-0.001	0.024	0.010	-0.001	0.076

Sampling point 4	0.016	0.055	0.009	0.016	0.067
Sampling point 5	0.016	0.052	0.008	0.012	0.059
Sampling point 6	0.058	0.112	0.011	0.057	0.088
Sampling point 7	-0.004	0.0489	0.013	-0.004	0.082
Sampling point 8	0.006	0.044	0.013	-0.013	0.130
Sampling point 9	-0.033	-0.002	0.007	-0.033	0.083
Sampling point 10	0.018	0.048	0.010	0.018	0.059
Sampling point 11	0.040	0.071	0.014	0.040	0.059
Sampling point 12	-0.011	0.019	0.005	-0.011	0.062

505

506 The test results show that in the system error of the test device, $\overline{\mu_B}$, was basically zero,
 507 m_B did not exceed 0.12 mm, σ_B did not exceed 0.014 mm, R_B did not exceed 0.057 mm,
 508 and D_B did not exceed 0.13 mm. Thus, the test device had high accuracy and precision.

509 Fig. 17 shows the distribution of the error data. The horizontal axis represents the sampling
 510 sequence, and the vertical axis represents the measurement error in millimeters.



511

512

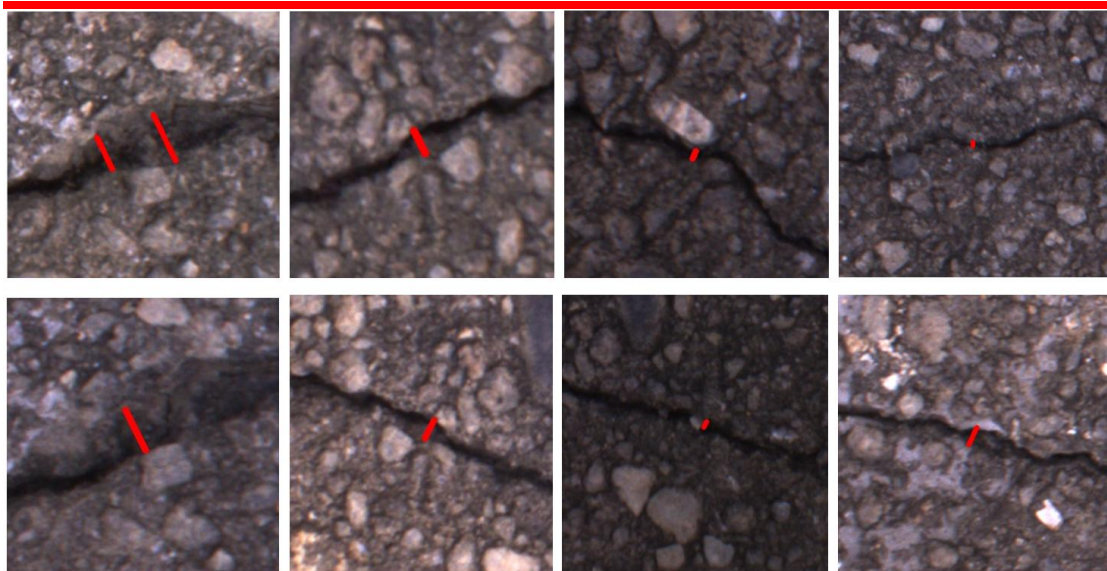
Fig. 17 Error distribution of repeated measurement sampling

513

514 3.6 Field width measurement test

515 The frame of the visual measurement test platform was constructed using aluminum profiles.
516 The main equipment included two MV-EM510C industrial cameras (resolution $2,456 \times 2,058$), the
517 focal length of the lens was 8 mm, and the distance between the camera lens and the dam surface
518 was approximately 240 mm. When installed, the visual axis was perpendicular to the surface of
519 the dam. A digital vernier caliper with an accuracy of 0.01 mm was used to measure the crack
520 width on site for comparison data. The proposed algorithm for determining the measurement
521 direction was used to obtain the measurable points in the crack. Then, five of the measurable
522 points were randomly selected for width measurement, and the measurement position was marked
523 in the real-time image of the left camera. Subsequently, the digital display vernier caliper was used
524 to measure the inner diameter of the crack to obtain the standard value of its width at that location,
525 as shown in Fig 18. The visual measurement value was used for comparison with the standard
526 value. Referring to the experiments in previous studies [26,43,45], the absolute error was used to
527 measure the accuracy of the proposed measurement method.

528



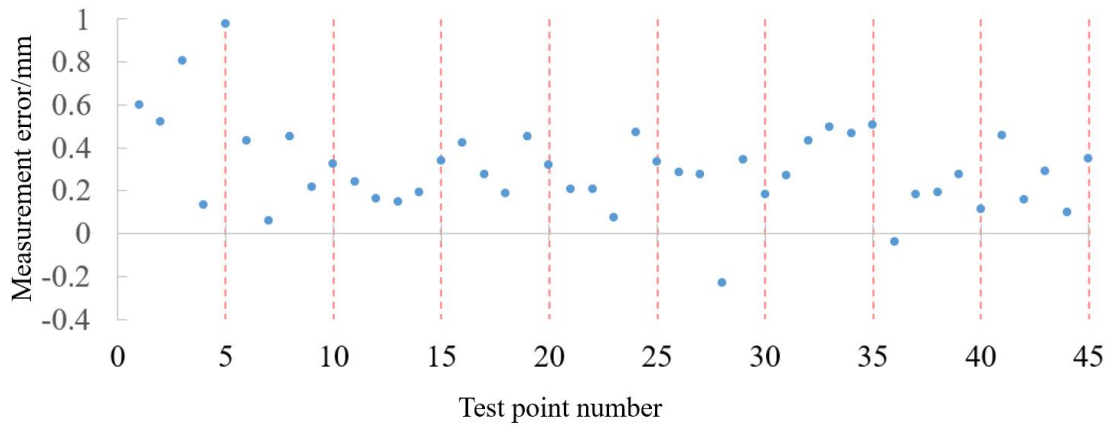
529

530

Fig. 18 Field measurement test

531

532 A total of nine groups were measured in this experiment. The deviation between the width
 533 value measured by the visual measurement and the standard value measured by the digital vernier
 534 caliper is shown in Fig. 19. The average absolute error, $\bar{\mu}$, and the standard deviation, σ , of the
 535 absolute error of each group of data are shown in Table 6.



537
 538 Fig. 19 Deviation of the width value of the visual measurement from the standard value

539
 540 Table 6. Width measurement error average and standard deviation

Group	Error/(mm)	$\bar{\mu}$ /(mm)	σ /(mm)	Group	Error/(mm)	$\bar{\mu}$ /(mm)	σ /(mm)
1	0.60	0.61	0.32	6	0.28	0.26	0.06
	0.52				0.28		
	0.81				-0.23		
	0.13				0.35		
	0.98				0.18		
2	0.43	0.30	0.16	7	0.27	0.43	0.10
	0.06				0.43		
	0.45				0.50		
	0.22				0.47		
	0.33				0.51		
3	0.24	0.22	0.09	8	-0.04	0.16	0.09

	0.16				0.18			
	0.15				0.19			
	0.19				0.28			
	0.34				0.11			
	0.42				0.46			
	0.28				0.16			
4	0.19	0.33	0.11	9	0.29	0.27	0.14	
	0.45				0.10			
	0.32				0.35			
	0.21							
	0.21				$\bar{\mu}$ mean = 0.32 mm			
5	0.07	0.26	0.15					
	0.47							
	0.34				σ mean = 0.19 mm			

541

542 In Fig. 19 and Table 6, the results show that the average error of this test was approximately
543 0.32 mm, and the average variance was 0.19 mm. This demonstrates that the visual measurement
544 test results in this study are close to those of commonly used methods in engineering, which
545 indicates that the proposed method can be utilized in engineering applications.

546

547 4 Conclusion

548 This study proposed a practical and complete visual method for measuring crack width using
549 a real dam as the research object. The effectiveness of U-Net in the task of crack segmentation
550 was first verified. Then, to address the problem of data redundancy in the crack skeleton, this
551 study designed a more streamlined and stable crack backbone extraction method. The total number
552 of eight-neighborhood points of each point on the backbone did not exceed two, which reduced
553 the amount of backbone data and the distribution types of the eight neighborhoods of backbone

1 554 points. The backbone's ability to describe the shape of cracks was also enhanced. Furthermore, we
2 555 designed a more accurate method for determining the direction of the crack width measurement by
3
4 556 combining the slope characteristics at the backbone macroscale feature and the neighborhood
5
6 557 distribution characteristics at the microscale feature. We further defined the crack width visual
7
8 558 measurement method according to the measurement direction.
9

10 559 To evaluate the advantages and disadvantages of the measurement methods, two criteria (i.e.,
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12 560 recall rate of measurement direction and direction error) were added to provide a technical
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14 561 reference for subsequent research. Then, we conducted a series of experiments to verify that the
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16 562 proposed crack backbone extraction algorithm has a good streamlining effect compared to the
17
18 563 Zhang–Suen image-refinement algorithm. Compared with the method presented by Luo et al. [46],
19
20 564 we demonstrated that our proposed method obtains a more accurate width measurement direction.
21
22 565 From the width measurement test, we also demonstrated that it has prospects for practical
23
24 566 engineering applications, and the intelligent degree of structural health monitoring and repair was
25
26 567 improved. The proposed method also provides a reference for the radial vision measurements of
27
28 568 other slender and irregular targets.
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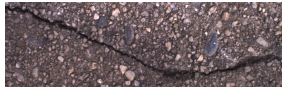



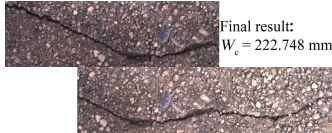

31 569 In the future, for structural damage (e.g., cracks), research on faster, lighter, more accurate,
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33 570 and more stable image segmentation methods based on U-Net is needed. The visual measurement
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35 571 process should also be streamlined on the basis of the existing framework to improve the
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37 572 efficiency of the algorithm. Finally, the three-dimensional reconstruction of cracks should be
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39 573 explored to improve measurement accuracy and depth measurements so that vision systems will
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41 574 inherit more comprehensive crack-damage detection capabilities.
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45 576 **Acknowledgments**

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47
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55

56 582 **Appendix A. Examples of processing procedures**

Process	Result	Process	Result
Original		Binarized by U-Net	
Backbone refinement		Curve fitting in Macro scale	
Distance to measuring surface		Width measurement	
P1(783, 1023)	Measurement point 1: (788,1013); Measurement point 2: (778,1033);	Measurement direction: 67.5° Width = 1.936 mm	
P2(1742, 1143)	Measurement point 1: (1731,1121); Measurement point 2: (1749,1158);	Measurement direction: 112.5° Width = 3.563 mm	
P3(1808, 1119)	Measurement point 1: (1796,1095); Measurement point 2: (1822,1148);	Measurement direction: 112.5° Width = 5.112 mm	
P4(2242, 1126)	Measurement point 1: (2242,1117); Measurement point 2: (2242,1140);	Measurement direction: 90° Width = 1.992 mm	
P5(2446, 1147)	Measurement point 1: (2446,1138); Measurement point 2: (2446,1156);	Measurement direction: 90° Width = 1.559 mm	

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1 Novel visual crack width measurement based on backbone double-scale features for 2 improved detection automation

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16 **Abstract:** State-of-the-art machine-vision systems have limitations associated with crack width
17 measurements. The sample points used to describe the crack width are often subjectively defined
18 by experimenters, which obscures the crack width ground truth. Consequently, in most related
19 studies, the uncontrollable system errors of vision modules result in unsatisfactory measurement
20 accuracy. In this study, the cracks of a reservoir dam are taken as objects, and a new crack
21 backbone refinement algorithm and width-measurement scheme are proposed. The algorithm
22 simplifies the redundant data in the crack image and improves the efficiency of crack-shape
23 estimation. Further, an effective definition of crack width is proposed that combines the
24 macroscale and microscale characteristics of the backbone to obtain accurate and objective sample
25 points for width description. Compared with classic methods, the average simplification rate of the
26 crack backbone and the average error rate of direction determination are all improved. The results
27 of a series of experiments validate the efficacy of the proposed method by showing that it can
28 improve detection automation and has potential engineering application.

29
30 **Key words:** Concrete crack; Image thinning; Machine vision; Multi-scale feature fusion

31 1 Introduction

32 Cracks are a common type of structural damage that jeopardize the health of concrete
33 buildings (e.g., roads, bridges, tunnels, and dams) [1–5]. Regular inspections and repairs can
34 reduce the risk of structural collapse during natural disasters (e.g., earthquakes and floods) [6–10].

1 35 Researchers have proposed a variety of innovative methods to replace traditional manual visual
2 36 inspection [11–14]. However, their methods target larger, more complex field-environment crack
3
4 37 detection tasks that are expensive, slow and susceptible to external interference [15–18].
5
6 38 Non-contact, high-precision computer-assisted visual measurement has shown good performance
7
8 39 in various inspection fields [19–23] and is a promising method to replace human visual
9
10 40 inspections. Researchers have provided a relatively complete process framework for mapping
11
12 41 image pixel features to geometric dimensions in real physical space [24,25]. However, for
13
14 42 complex slender and irregular targets, such as cracks, the current measurement applications lack
15
16 43 geometric meaning, and their accuracy is not sufficient [26].

18 44 Regarding the identification and segmentation of cracks, researchers have applied the classic
19
20 45 digital image processing (DIP) method and neural-network models to make the extraction of
21
22 46 cracks more robust [27–32]. Kim et al. [33] compared the threshold segmentation effects of five
23
24 47 classic threshold segmentation algorithms on concrete cracks and showed that the less robust
25
26 48 threshold segmentation suffers background complexity, large changes in illumination, and
27
28 49 inconsistencies. It is generally difficult to accurately detect cracks under uniform conditions. Other
29
30 50 researchers have proposed semantic segmentation models that have been effective in solving these
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32 51 problems [34–37]. Many scholars have also proposed corresponding model structures specifically
33
34 52 for crack detection. For example, Zou et al. developed the DeepCrack [27] network based on
35
36 53 SegNet and achieved an F-measure greater than 0.87. They improved the segmentation accuracy
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38 54 but introduced larger scale parameters. Ju et al. developed the CrackU-net [38] model, which
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40 55 improved on U-Net and FCN and achieved an accuracy of 99.01%. Wang and Cheng combined
41
42 56 DilaSeg and RNN and proposed DilaSeg-CRF [29] for segmentation cracks, which achieved a
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44 57 20% to 32% improvement compared to the classic semantic segmentation model. Zhang et al.
45
46 58 designed CrackNet [39] without a pooling layer in an attempt to reduce the accuracy loss in the
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48 59 crack segmentation process. Then, they combined it with an RNN and proposed CrackNet-R [28]
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50 60 to improve the accuracy of segmentation, subsequently obtaining a higher recall rate and
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52 61 F-measure. These neural-network methods were optimized for concrete cracks and provided more
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54 62 opportunities for improvement. However, increasing the network depth to improve accuracy
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63 increases the burden on the hardware in the application process.

64 The quantitative analysis of crack-hazard degree (e.g., crack length, width, and depth) is
65 presently insufficient [17,40]. For example, clearly defining a crack width from a visual
66 measurement and continuously performing such measurements remain quite challenging
67 [26,41,42]. Historically, researchers used an edge or a skeleton of the crack as the basis for width
68 measurement [43], but several problems remain. For example, the two edges of a crack may be
69 quite different in the local area, and it is difficult to obtain accurate measurement directions. The
70 crack skeletons obtained by improved refinement algorithms must still handle redundant data, and
71 the definition of the skeleton remains inaccurate.

72 Researchers have attempted to use these features to define the crack-width visual
73 measurement method and achieved varying results. For example, Asjod et al. [44] proposed the
74 arc-length method to measure cracks. Further, Wang et al. [26] proposed a Laplace-based
75 continuous explicit measurement method that simulates the crack as an electric field in a capacitor,
76 and used the total length of the trajectory of electrons in the cathode and anode of a capacitor to
77 define the width of the crack. However, the width obtained by their method is the length of a curve,
78 not a straight-line distance needed for engineering. Kim et al. [45] proposed using the two edge
79 points closest to the crack skeleton point for width measurement. Luo et al. [46] investigated the
80 crack edges from the crack skeleton point in four directions and took the minimum distance
81 between the two edges in the four directions as the width of the crack. Their method performs well
82 with idealized cracks. However, in reality, the width often refers to the straight-line distance
83 between the two edges in the normal direction of the crack-growth direction, and the crack edges
84 often have irregular bumps. Hence, the two edges are not strictly symmetrical about the skeleton.

85 The above methods use measurement points that do not match the geometric meaning of
86 width. Therefore, the measurement correctness must be improved. The comprehensiveness of
87 using only numerical results as the evaluation criteria of measurement methods needs to be
88 improved. In addition, whereas many studies have focused on road cracks, only a few have
89 focused on dam cracks, which have characteristics of large image noise, complex background
90 texture, and random location [47,48]. The research object needs to be expanded, thus, a large

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91 scope exists for machine-vision measurement research in this area.

92 In this study, we selected a reservoir dam crack located in the field as the research object and
93 developed a more streamlined crack backbone extraction algorithm, based on an improved
94 image-refinement algorithm, that enhances the backbone's ability to describe crack shapes. Further,
95 we devised a more accurate measurement direction by combining the backbone macroscale slope
96 characteristics and microscale neighborhood distribution characteristics. Then, defining the width
97 of the crack as the straight-line distance between two measurement points located at the edge of
98 the crack in the measurement direction, we developed a crack-width measurement method. Two
99 evaluation criteria are included: the measurement recall rate and direction error. Compared with
100 the method proposed by Luo et al. [46], the method proposed here is more comprehensive, in that
101 it has a more accurate visual measurement performance that aligns with the geometric meaning of
102 width. This study makes the following contributions:

103 1. A detailed visual crack width measurement process is proposed that can provide stable and
104 continuous measurements.

105 2. Based on the improved image-refinement algorithm used to further refine the complete
106 crack backbone, the neighborhood distribution types of backbone points are reduced to facilitate
107 their use in classifying backbone points.

108 3. Combining the macro and micro characteristics of the backbone, a visual crack width
109 measurement method that is closer to the actual needs of the project is used to obtain a more
110 accurate measurement method.

111 4. Two evaluation measurement standards (i.e., recall rate and direction error) are added to
112 enable a more comprehensive evaluation of the measurement method.

113 The remainder of this article is structured as follows. The process and principle of the crack
114 width measurement method are described in Section 2. Section 3 presents the relevant evaluation
115 test conducted on the proposed method. Section 4 provides concluding remarks and outlines
116 possible future study.

117 **2 Methods**

118 2.1 Visual crack-measurement process

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3 119 The basic processes of the width-measurement method proposed in this study include crack
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5 120 segmentation, backbone refining, and width measurement. The specific process is shown in Fig. 1.
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7 121 Previous studies have shown that the U-Net semantic segmentation model is sensitive to edge
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9 122 detail features, which also suggests that it would be suitable for dam-crack segmentation [49–52].
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11 123 In this article, the input into U-Net was an RGB image and the output is a semantically segmented
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13 124 binary image. The process of semantic segmentation takes place in a code-decoded symmetrical
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15 125 U-shaped structural model, hence the name U-Net. The acquisition of the parameters in the
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17 126 U-shaped structural model requires convolutional inference of a large number of labeled samples,
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19 127 the result of which is then recorded in the model file. When using U-Net, this model file is called
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21 128 and the image data is passed into the model. The segmentation result can be obtained after
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23 129 calculation by U-Net, which is a very simple and commonly used semantic segmentation model.
24
25 130 In this study, the results of the U-Net semantic segmentation model were therefore directly used as
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27 131 the input material for the pretreatment of the crack backbone extraction and crack width
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29 132 measurement. Pretreatment can effectively handle possible misjudgment problems in crack
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31 133 segmentation while improving the robustness of backbone refining. Morphology (large) represents
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33 134 the morphological processing of the large window, which is used for the segmentation of the crack
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35 135 area; morphology (small) represents small window morphology processing, which is used to
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37 136 strengthen the connectivity of the crack binary image. Morphological processing here refers to
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39 137 dilation or erosion algorithms (they have opposite effects to each other), whose role is to expand
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41 138 the binarized target towards the background. Combinatorial binarization is the combined operation
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43 139 of binarization–blur–binarization, which is used to smooth the crack binary image and eliminate
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45 140 segmentation impurities before backbone extraction. The role of blur is also to expand the target,
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48 141 but its effect is more moderate than that of morphological processing.
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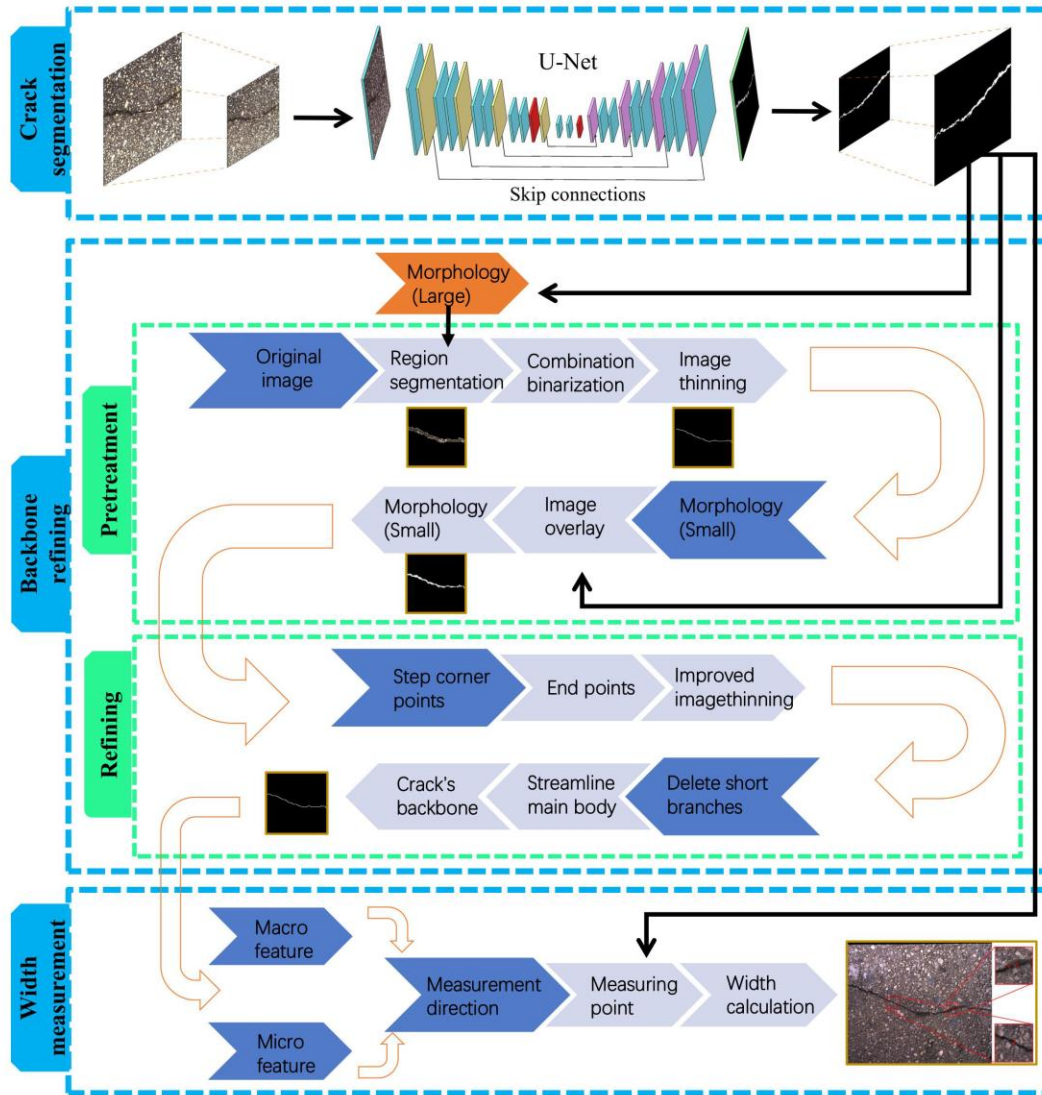


Fig. 1 Framework and flowchart for visual measurement

2.2 Crack backbone refinement

To address the problem of redundant data points when the image-refinement algorithm extracts the crack skeleton, we refine the crack skeleton and the backbone of the crack using the improved image-refinement algorithm to mark the ends of the cracks while avoiding end-shortening during refinement. The refinement of the crack backbone removes redundant points on the branches and backbones based on the skeleton.

The backbone of the crack contains information on the shape of the crack, which has the

152 function of determining its position and providing the basis for measuring its width. The classic
 153 Zhang–Suen image thinning algorithm [53] can be used to extract the crack skeleton, but the
 154 skeleton still has redundant data, which can be further streamlined to obtain the backbone of the
 155 crack. For the convenience of comparison and explanation in this work, it is stipulated that the
 156 output of the Zhang-Suen image thinning algorithm is called “skeleton”, and the output proposed
 157 for improvement and further processing based on the Zhang-Suen image thinning algorithm is
 158 called “backbone”.

159 The input into the crack backbone refinement algorithm is a crack binary image with only
 160 crack and background pixels. This process involves iterative refinement. In each iteration, the
 161 outermost contour is transformed into the background. The algorithm sets a certain crack pixel as
 162 P_0 . Starting from the pixel just above P_0 , the eight neighborhoods of P_0 are set as P_1 to
 163 P_8 , clockwise. The background point is assigned a value of either zero or one, as shown in Fig.
 164 2.

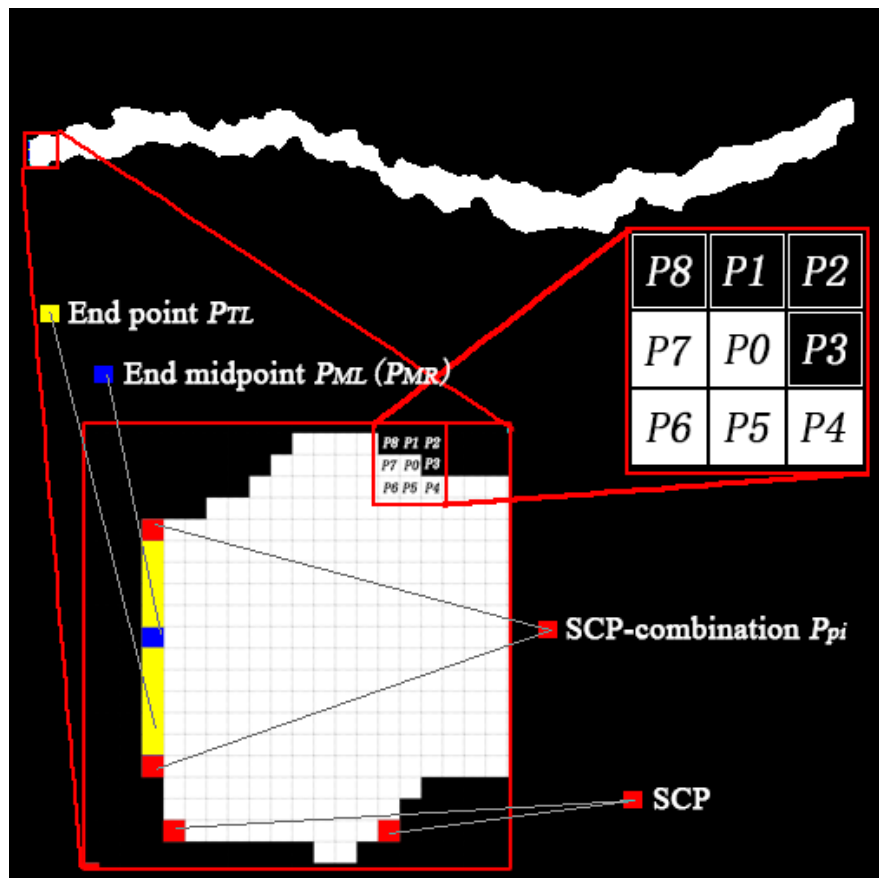


Fig. 2 Feature points in crack binary graph

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168 Detecting the edge of the crack binary image involves multiple steps. As shown in Fig. 2,
 169 each step with a vertex height greater than 1 pixel is the step corner point (SCP), which can be
 170 found according to its eight-neighborhood features and is used to build set CoP . Let $P_0(\Delta P)$
 171 denote the set of P_0 's eight neighborhoods satisfying condition ΔP . The set, CoP , is given by
 172 the formula $CoP = \{P_0 | P_0(\Delta P)\}$, in which ΔP is defined by Eq. (1):

$$\begin{aligned}
 & \exists(P_1 + P_2 + P_3 = 3 \wedge P_5 + P_6 + P_7 + P_8 = 0) \\
 & \vee(P_3 + P_4 + P_5 = 3 \wedge P_1 + P_6 + P_7 + P_8 = 0) \\
 & \vee(P_5 + P_6 + P_7 = 3 \wedge P_1 + P_2 + P_3 + P_4 = 0) \\
 & \vee(P_7 + P_8 + P_1 = 3 \wedge P_2 + P_3 + P_4 + P_5 = 0), \quad P_0 \in P_0(\Delta P)
 \end{aligned} \tag{1}$$

174 In CoP , the two SCPs in the same column are recorded as a set, P_{pi} , and its midpoint,
 175 P_{piM} , is marked from there, as shown in Fig. 2. Then, according to the eight-neighborhood
 176 feature, the P_{piM} in the left and right ends of the crack, which are regarded as P_{ML} and P_{MR} ,
 177 can be separated from the set of all P_{piM} . P_{ML} and P_{MR} 's eight neighborhoods at the left and
 178 right ends to satisfy Eq. (2).

$$\begin{aligned}
 & (a) P_6 + P_7 + P_8 = 0 \Rightarrow P_{ML} \\
 & (b) P_2 + P_3 + P_4 = 0 \Rightarrow P_{MR}
 \end{aligned} \tag{2}$$

180 The pixels in the same column as P_{ML} or P_{MR} are the crack's end points—recorded as P_{TL}
 181 and P_{TR} , respectively. If P_{TL} and P_{TR} 's eight neighborhoods satisfy the condition $P_1 + P_5 = 2$,
 182 they are respectively recorded in sets $TePL$ and $TePR$. The purpose of this move is to eliminate
 183 the points overlapping the edges among the endpoints during the refinement process.

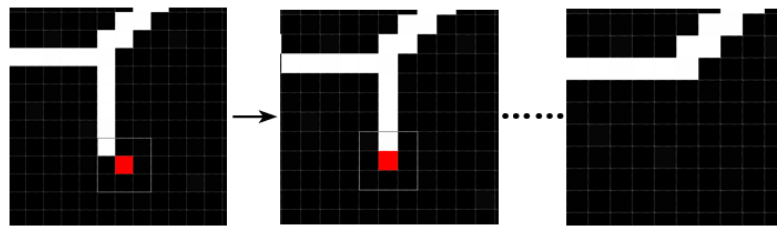
184 Let $A(P_0)$ denote the number of 01 patterns of the clockwise connections in the eight
 185 neighborhoods of P_0 and $B(P_0)$ denote the number of crack pixels in the eight neighborhoods
 186 of P_0 . One iteration of the crack backbone extraction algorithm is divided into odd- and
 187 even-numbered sub-iterations. In each sub-iteration, the crack pixels that satisfy Eq. (3) are

188 marked as the outermost pixels, which are uniformly converted into background pixels before the
 189 iteration completes. In even-numbered sub-iterations, only conditions (c), (d), and (e) are
 190 respectively changed to (c'), (d'), and (e').

$$\begin{aligned}
 & (a) A(P_0) = 1 \\
 & (b) 2 \leq B(P_0) \leq 6 \\
 & (c) P_1 \times P_3 \times P_5 = 0 \\
 191 & (d) P_3 \times P_5 \times P_7 = 0, \\
 & (e) P_0 \notin TePR \\
 & (c') P_1 \times P_3 \times P_7 = 0 \\
 & (d') P_1 \times P_5 \times P_7 = 0 \\
 & (e') P_0 \notin TePL
 \end{aligned} \tag{3}$$

192 The algorithm iteratively thins the cracks to obtain the skeleton according to the above rules
 193 until no crack pixels are marked as outermost pixels. However, there are still numerous redundant
 194 points in the skeleton that can be streamlined further. The streamlining process is divided into two
 195 steps: deleting short branches and streamlining the skeleton's main body to obtain the backbone.

196 To delete short branches, the skeleton's endpoints are marked on the left and right sides of the
 197 image and other endpoints satisfying $B(P_0) < 2$, or $B(P_0) = 2$ and $A(P_0) = 1$, apart from the
 198 skeleton's endpoints. Once an end point is deleted on the short branch, the connected point
 199 becomes the new endpoint. These operations are repeated several times until all short branches are
 200 deleted. The deletion process is illustrated in Fig. 3.



201
 202 Fig. 3 Short branch deletion process

203 The refinement of the backbone is to convert pixels in the skeleton line that satisfy any of the
 204 items in Eq.(4) to the background. If the image is scanned from the first pixel in the upper left
 205 corner to the last pixel in the lower right corner, then, as shown in Fig. 4, the red pixels are deleted.
 206 After cleaning, the backbone is obtained with the following features:

207 (1) The total number of backbone pixels in each point's eight-neighborhood does not exceed

208 2.

209 (2) Its eight-neighborhood pixel distribution will show four shapes: v shape, linear shape,

210 semi-Y shape of left and semi-Y shape of right. Plus, when each shape is rotated around the center,

211 the number of neighborhood distribution types of backbone points is reduced to

212 $C_4^2 + C_2^1 + C_4^1 C_2^1 = 16$, as shown in the lower right corner of Fig. 4.

$$\begin{aligned}
 & (a) P_1 + P_3 = 2 \\
 & (b) P_1 + P_7 = 2 \\
 & (c) P_5 + P_3 = 2 \\
 & (d) P_5 + P_7 = 2
 \end{aligned} \tag{4}$$

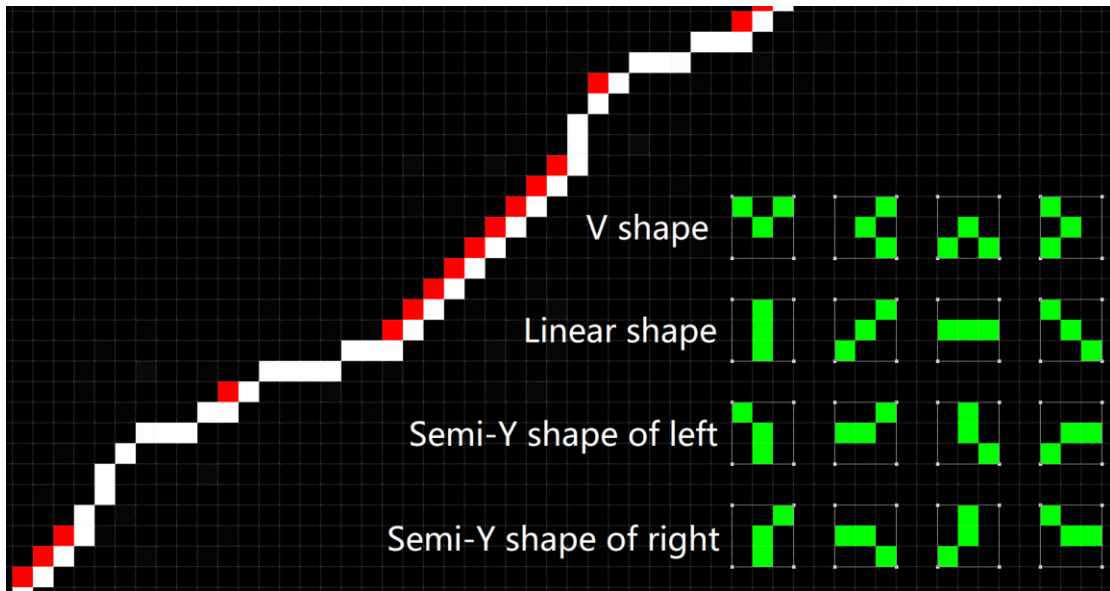


Fig. 4 Streamlined backbone

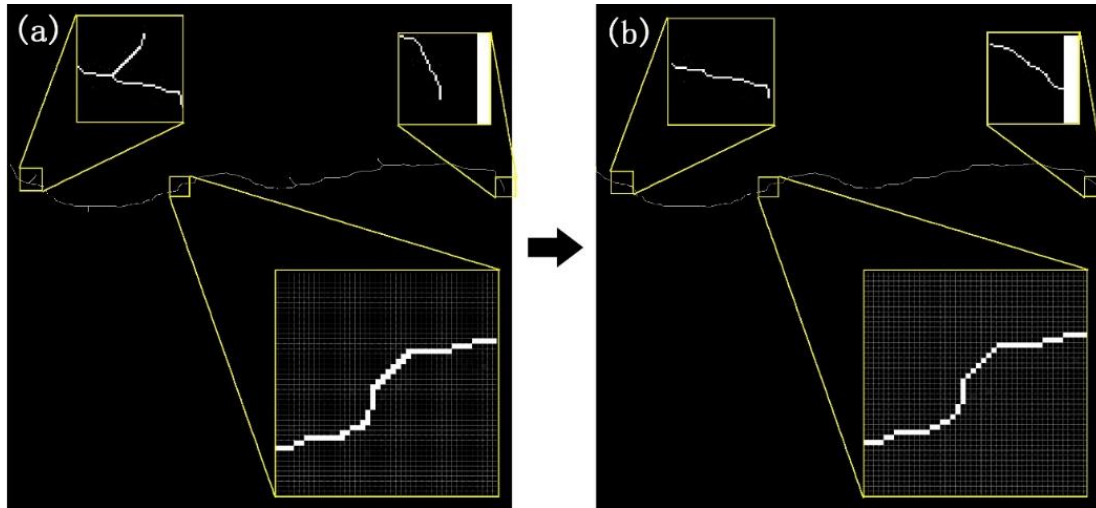
216 Fig. 5 illustrates the effect of the main crack extraction. The backbone extraction algorithm in
 217 this paper is more streamlined than others. In total, compared with the classic Zhang-Suen image
 218 thinning algorithm, the crack backbone refinement algorithm in this paper has the following
 219 characteristics:

220 1. The branches are removed and the shape of the end of the crack is retained (as shown in
 221 the upper left corner of Fig. 5a and upper right corner of Fig. 5b);

222 2. The eight-neighborhood effective pixels of the backbone do not exceed 2 and there are

223 only 16 types of neighborhood pixel distribution (as shown in the lower right corner of Fig. 4 and
224 the lower right corner of Fig. 5).

225 While simplifying the amount of data, it is convenient to use the neighborhood distribution
226 type to classify the backbone points, which is conducive to the subsequent clear definition of the
227 crack-width measurement.



228
229 Fig. 5 Classic thinning algorithm (a) compared with the improved backbone refining
230 algorithm in this study (b)
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232 2.3 Determining the crack width measurement direction

233 As shown in Fig. 6, there are multiple measurement schemes that rely on the same
234 measurement position, O. The measurement schemes AE, BF, CG and DH are the
235 width-measurement results obtained at position O in different measurement directions. Notably,
236 they are quite different from each other. The width is measured along the normal direction of the
237 crack-growth direction according to the visual inspection method commonly used by engineers in
238 practice. Evidently, the solution BF is more suitable for characterizing the width of the crack at
239 position O. The main objective of this section is to get as many measurement points as possible
240 and determine the width of the crack in the visual measurement along the optimum measurement
241 direction to closely approximate the width obtained by the commonly used method in practice.



Fig. 6 Different measurement methods on the same crack

This paper proposes a method for determining the direction of crack width measurement based on the dual-scale features of the backbone. The proposed method combines the slope information of the crack backbone at the macroscale with its neighborhood information at the microscale. The macroscale information is based on the trend of the entire backbone of the crack, whereas the microscale information is based on the neighborhood distribution information of each pixel of the crack backbone. The combined method defines eight measurement directions, and then macro- and micro-scale information is matched to each of these eight directions. When the dual-scale information matches, the measurement direction can be determined and obtained. For points where the macroscale and microscale information do not match, the measurement is abandoned. Because the point where the direction is incorrect or cannot be measured will affect the reliability of the measurement result.

At the macro level, this study uses the least-squares method to fit the n-degree polynomial curve of the main stem into a polynomial function, $v = f(u)$, as established in Eq. (5):

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$$\begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_m \end{bmatrix} = \begin{bmatrix} 1 & u_1 & \cdots & u_1^n \\ 1 & u_2 & \cdots & u_2^n \\ \vdots & \vdots & \ddots & \vdots \\ 1 & u_m & \cdots & u_m^n \end{bmatrix} \times \begin{bmatrix} w_1 \\ w_2 \\ \vdots \\ w_n \end{bmatrix} \quad (5)$$

$$\mathbf{V} = \mathbf{U} \times \mathbf{W}$$

259 where (u_m, v_m) is the coordinate value of the backbone point in the image coordinate system, W
 260 is the coefficient matrix of the polynomial function, m is the number of backbone points
 261 participating in the polynomial curve-fitting, n is the order of the highest degree of the curve,
 262 and $n = 9$.

263 The least-squares method is used to solve matrix W , as shown in Eq. (6):

$$\mathbf{W} = (\mathbf{U}^T \mathbf{U})^{-1} \mathbf{U}^T \mathbf{V}. \quad (6)$$

265 The first-order derivative of the function can be used to obtain the slope, dv_m , at any point
 266 on the backbone, as shown in Eq. (7):

$$dv_m = \sum_{i=1}^n a_{n-i} u_m^{n-i-1}. \quad (7)$$

268 The angle, θ , between a straight line passing through any backbone point and the horizontal
 269 axis represents the measurement direction. This study defines eight measurement directions with
 270 an interval of 22.5° between each. At the macro level, mapping is defined from the slope, dv_m , of
 271 the curve, $v = f(u)$, to the macro measurement direction, ϕ , as shown in Eq. (8).

$$\phi = \begin{cases} 0^\circ, dv_m \in (-\infty, \tan 101.25^\circ) \cup [\tan 78.75^\circ, +\infty) \\ 22.5^\circ, dv_m \in [\tan 101.25^\circ, \tan 123.75^\circ) \\ 45^\circ, dv_m \in [\tan 123.75^\circ, \tan 146.25^\circ) \\ 67.5^\circ, dv_m \in [\tan 146.25^\circ, \tan 168.75^\circ) \\ 90^\circ, dv_m \in [\tan -11.25^\circ, \tan 11.25^\circ) \\ 112.5^\circ, dv_m \in [\tan 11.25^\circ, \tan 33.75^\circ) \\ 135^\circ, dv_m \in [\tan 33.75^\circ, \tan 56.25^\circ) \\ 157.5^\circ, dv_m \in [\tan 56.25^\circ, \tan 78.75^\circ) \end{cases}. \quad (8)$$

273 At the microscale, there are only 16 types of eight-neighborhood distributions of backbone
 274 points, and the number is relatively small. The mapping from the backbone point to the microscale

275 measurement direction, φ , can be defined according to the eight-neighbor distribution types, as
 276 shown in Eq. (9).

$$277 \quad \varphi = \begin{cases} 0^\circ, (p1 + p5 = 2) \vee (p6 + p8 = 2) \vee (p2 + p4 = 2) \\ 22.5^\circ, (p1 + p4 = 2) \vee (p5 + p8 = 2) \vee (p1 + p5 = 2) \\ 45^\circ, (p4 + p8 = 2) \vee (p1 + p4 = 2) \vee (p5 + p8 = 2) \\ 67.5^\circ, (p4 + p7 = 2) \vee (p3 + p8 = 2) \vee (p3 + p7 = 2) \\ 90^\circ, (p3 + p7 = 2) \vee (p4 + p6 = 2) \vee (p2 + p8 = 2) \\ 112.5^\circ, (p2 + p7 = 2) \vee (p3 + p6 = 2) \vee (p3 + p7 = 2) \\ 135^\circ, (p2 + p6 = 2) \vee (p1 + p6 = 2) \vee (p2 + p5 = 2) \\ 157.5^\circ, (p1 + p6 = 2) \vee (p2 + p5 = 2) \vee (p1 + p5 = 2) \end{cases} . \quad (9)$$

278 In fact, using only the macro- or micro-scale information of the backbone for direction
 279 determination may cause a large direction error. On the one hand, the polynomial curve fitted at
 280 the macroscale is continuous and smooth, and it is difficult to accurately fit the growth
 281 morphology of the crack backbone, as shown in Fig. 7; the white dots constitute the crack's
 282 backbone and the orange line is the smooth curve after fitting. They do not exactly coincide. On
 283 the other hand, at the microscale, as shown in the lower left corner of Fig. 4, only three pixels are
 284 used as the basis for direction determination at a time, which is insufficient to express the current
 285 growth state of the crack. In the blue circle in Fig. 7, manual measurement should be carried out in
 286 the 45° direction. However, as shown in the red circle, if microscale information has been used for
 287 measurements, it is measured in the vertical direction. Similarly, in the green circle, the vertical
 288 direction should be followed when taking the manual measurement. However, as shown in the
 289 yellow circle, if macroscale information has been used, it is still measured in the 45° direction.

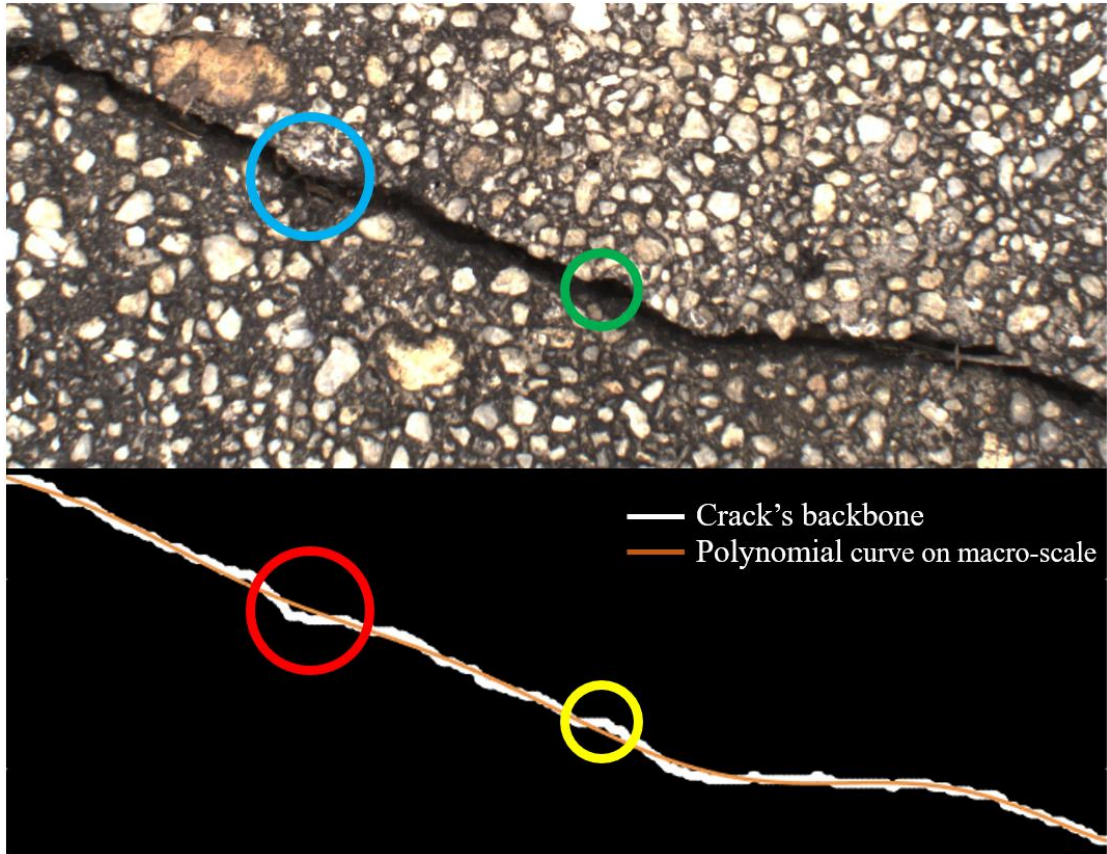


Fig. 7 Polynomial curve vs crack's backbone

Therefore, the measurement direction determination method must be designed to avoid errors in direction determination when using macroscopic or microscopic scale information alone. When solving the microscale direction, φ , this method is a situation where there are multiple neighborhood distribution types corresponding to one direction. Therefore, the microscale direction φ can be seen as a constraint on the macroscale direction, ϕ . When the macroscale, ϕ , and microscale, φ , directions of the backbone point are equal, the measurement direction, θ , of the point can be expressed as $\theta = \phi = \varphi$.

2.4 Crack width measurement

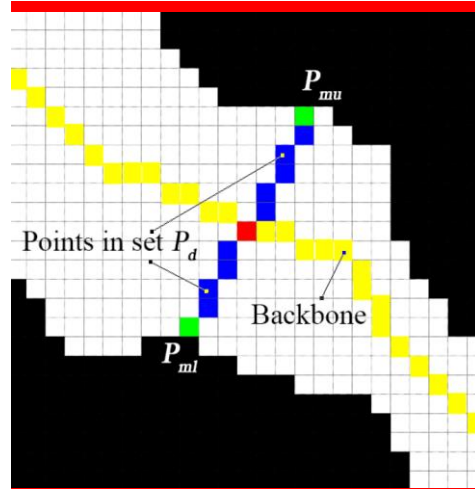
The straight line measurement, L_m , is defined according to the measurement direction and the main point, and the crack point (u_i, v_i) closest to L_m is found to form a point set, P_d , as in

302 Eq. (10):

$$303 \quad P_d = \{(u_i, v_i) \mid |v_i - (\tan \theta * u_i + b)| < 1\}, \quad (10)$$

304 where b is the intercept of the linear equation, which can be obtained by substituting the
 305 coordinates of the backbone point into the equation.

306 The set P_d includes the upper edge measurement point, P_{mu} , and the lower edge
 307 measurement point, P_{ml} , of the crack. As shown in Fig. 8, the yellow dots indicate the crack's
 308 backbone, the red dot is the measurement position at that place, the blue dots are P_d , and the
 309 green pixels are the two measurement points found according to the above method.



310
 311 Fig. 8 Acquisition process for the measuring points

312
 313 The values of P_{mu} and P_{ml} are shown in Eqs. (11) and (12):

$$314 \quad P_{mu} \begin{cases} (u_{max}, v_{min}), 0^\circ \leq \theta < 90^\circ \\ (u_{min}, v_{min}), 90^\circ \leq \theta < 180^\circ \end{cases}, \quad (11)$$

$$315 \quad P_{ml} \begin{cases} (u_{min}, v_{max}), 0^\circ \leq \theta < 90^\circ \\ (u_{max}, v_{max}), 90^\circ \leq \theta < 180^\circ \end{cases}. \quad (12)$$

316 As shown in Fig. 9, the blue line indicates the measurement method of the proposed method
 317 at this location, and the cracks covered by the blue lines can represent the range that can be
 318 measured on the crack image of this scheme.



Fig. 9 Measurable point of a section of a crack and its measurement scheme

In this study, a binocular vision system is used for width-vision measurement, and the camera's sight axis is set perpendicular to the dam surface. Before measurement, the camera must be double-targeted to correct distortion and to perform epipolar line correction between the two cameras. Template matching is used to obtain four 50×50 image blocks on the right image corresponding to the upper-left, lower-left, upper-right, and lower-right of the left image. A four-dimensional vector, $\mathbf{uB}_i = [u_{Li} \quad v_{Li} \quad u_{Li} - u_{Ri} \quad 1]^T$, is constructed for the center of each image block $(u_{Li}, v_{Li})^T$, representing the coordinates of the center point of the image block on the left image in the image coordinate system. $u_{Li} - u_{Ri}$ represents the disparity value, d , of the center point of the same image block on the left and right images. The triangulation principle, $\mathbf{CB} = \mathbf{Q} \times \mathbf{uB}$, is used to obtain the coordinates, $\mathbf{CB}_i = (X_{Ci}, Y_{Ci}, Z_{Ci}, W_i)^T$, of the centers of the four image blocks in the camera coordinate system. \mathbf{Q} is the reprojection matrix, which is obtained by the camera's dual objective setting, and \mathbf{W} is a constant. The average of the four depth values indicates the average depth of the camera's optical center from the dam surface. Equation (13) is used to calculate the crack width, W_c , represented by the two measurement points,

$$P_{mu}(u_{mu}, v_{mu}) \text{ and } P_{md}(u_{md}, v_{md}).$$

$$W_c = \frac{\bar{Z}}{f_x \cdot f_y} \sqrt{f_y^2 \cdot (u_{mu} - u_{md})^2 + f_x^2 \cdot \pi (v_{mu} - v_{md})^2}. \quad (13)$$

338 Between these, f_x and f_y are the internal parameters of the camera, which represent the
339 product of the physical focal length of the lens and the size of each unit in the x and y directions of
340 the imaging device, respectively, which are obtained by camera calibration.

341 **3 Test results and analysis**

342 The test site of this study was Fenghuang Reservoir Dam in Conghua District, Guangzhou
343 City, Guangdong Province. The dam of this reservoir has obvious cracks, and the samples are
344 abundant. The test site is shown in Fig. 10.

345 For the crack backbone extraction algorithm, we set the reduction rate test to illustrate the
346 performance of the algorithm when reducing the amount of data. To measure the performance of
347 the direction determination method, we used the two evaluation criteria proposed in this study: the
348 recall rate of the direction determination and the direction error, and the corresponding judgment
349 method. A segmentation performance evaluation test and a width-vision measurement accuracy
350 test were conducted. For the ground truth, we referred to the experiment in Section 4.2 of [26]. Six
351 researchers marked the cracks; the direction of the crack width was the tangent direction of the
352 commonly used crack growth, and the width was the distance between two points on the edge of
353 the crack in the measurement direction.



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355
356 Fig. 10 Test equipment and environment

357 **3.1 Segmentation performance evaluation**

358 A total of 5,760 sample images were used for training, all samples were randomly arranged,

1 359 and the training, validation, and test sets were randomly allocated at a ratio of 6:2:2. For the
2 360 training input and prediction output of the model, a square image with a resolution of 400×400
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4 361 pixels was used. The Adam optimization algorithm was used in all relevant procedures.
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6 362 For the trained U-Net model, commonly used semantic segmentation evaluation indicators
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8 363 were used (i.e., pixel accuracy [PA], average pixel accuracy [MPA], average intersection and
9 364 combination ratio [MioU], and frequency weight intersection and combination ratio [FWIoU]) to
10 365 evaluate the performance of U-Net segmentation for dam-crack evaluation. The evaluation was
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12 366 based on a test set having 1,152 images of dam cracks. The segmentation results of the model
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14 367 were decomposed to the original size of the test images via linear interpolation.
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18 368 To evaluate the segmentation effect of U-Net, the crack segmentation effects of the common
19 369 semantic segmentation networks, SegNet and DeeplabV3+ (with Xception and MobileNetv2 as
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21 370 the backbone networks, respectively), were added for comparison. The distributions of their
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23 371 performance evaluation scores are shown in Fig. 11, while visual comparisons are presented in Fig.
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25 372 12. The abscissa is the order of the graph, and the ordinate is the score.
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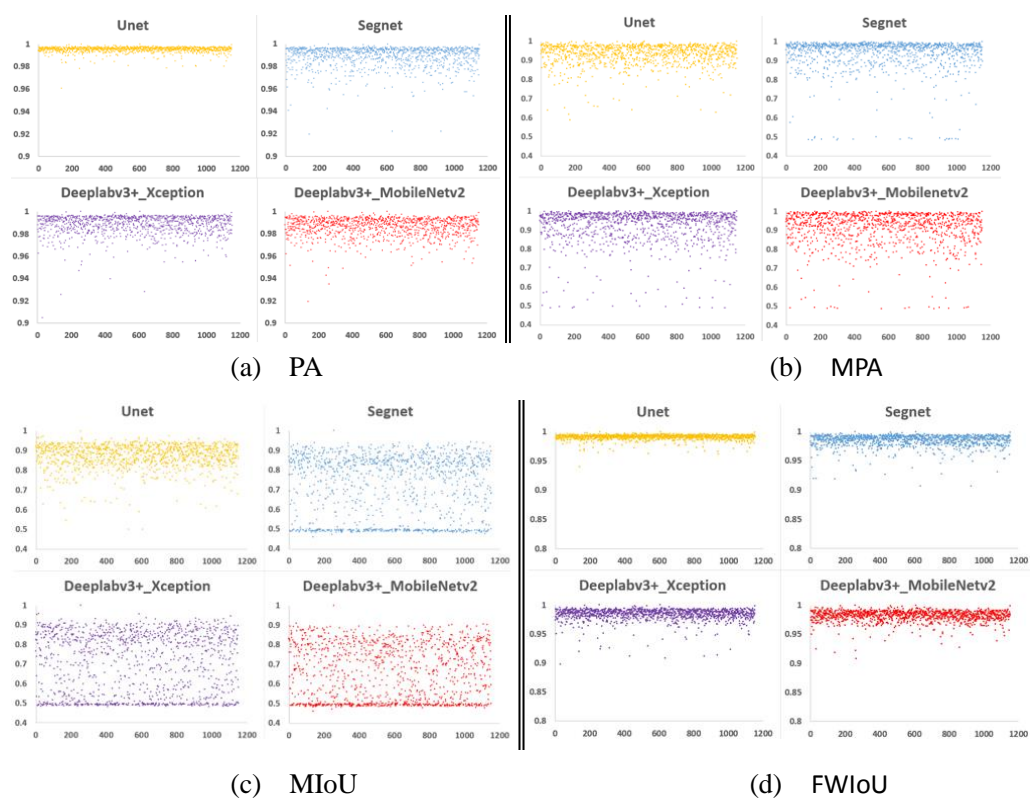


Fig. 11 Distribution comparison of the crack segmentation performance scores

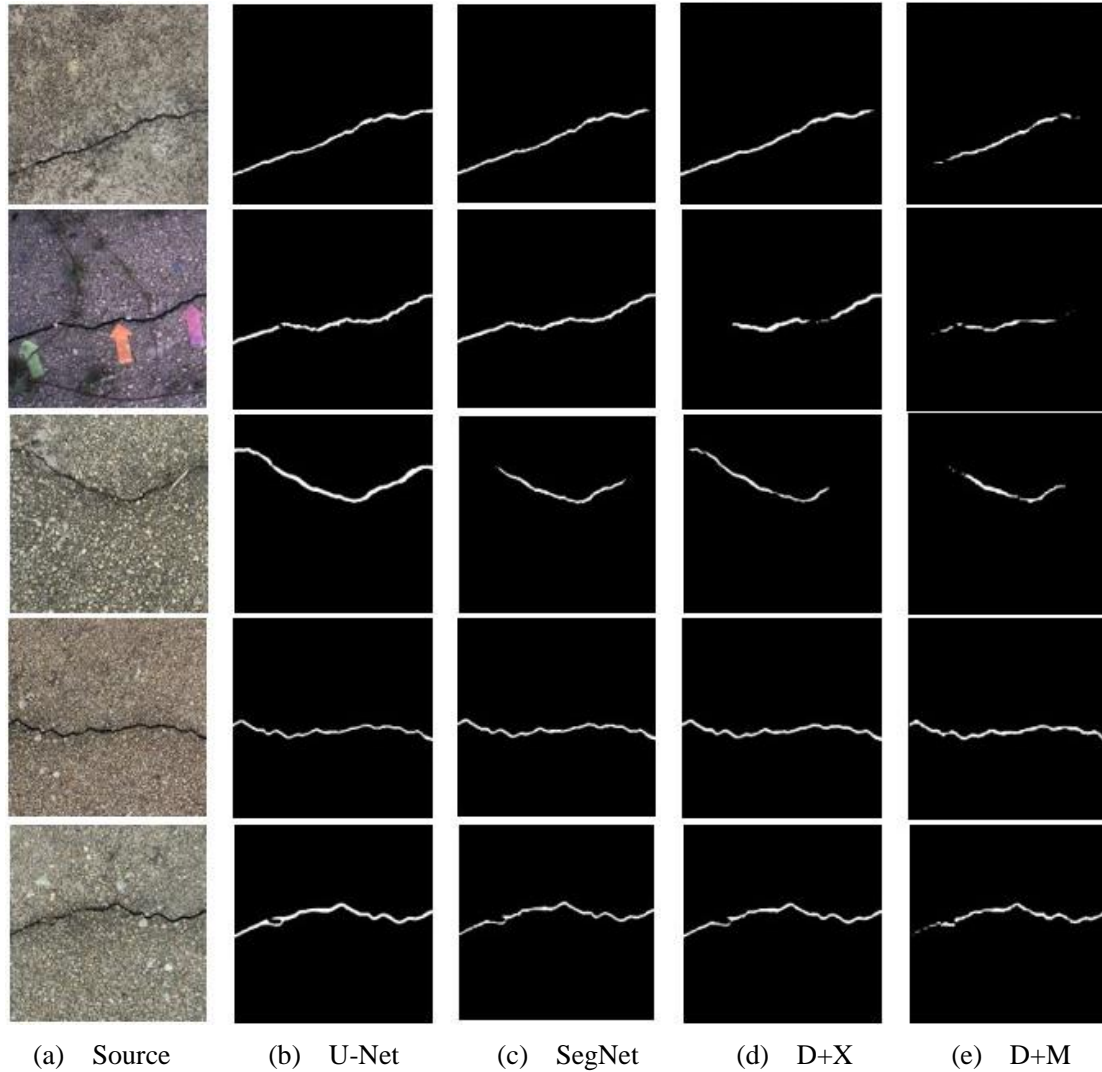


Fig. 12 Visual comparison of segmentation effects

The statistical results of the average and standard deviations of the performance evaluation scores are shown in Table 1.

Table 1. Statistics of the average and standard deviation of U-net performance evaluation scores

	PA		MPA		MIoU		FWIoU	
	Average	S.D.	Average	S.D.	Average	S.D.	Average	S.D.
U-Net	99.5 %	0.003	93.1 %	0.054	87.1 %	0.062	99.1 %	0.005
SegNet	98.9%	0.009	93.5%	0.084	72.5%	0.153	98.5%	0.010
D+X	98.8%	0.009	92.1%	0.087	70.8%	0.154	98.4%	0.011
D+M	98.6%	0.009	91.1%	0.089	65.8%	0.139	98.2%	0.010

* D+X is Deeplabv3+ with the backbone network of Xception, while D+X is MobileNetv2.

The results show that U-Net has higher segmentation accuracy and stability in the task of

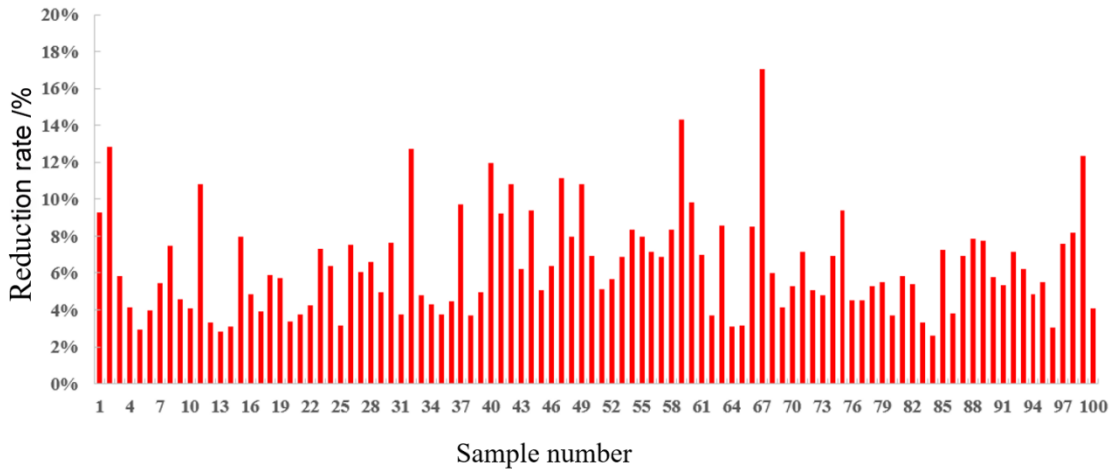
391 segmenting dam cracks than the other networks. Thus, a better improvement plan based on U-Net
 392 would be worthwhile. Consequently, U-Net segmentation results were directly used for
 393 subsequent width measurement in this study.

394 3.2 Evaluation of streamlining performance of crack backbone extraction algorithm

395 In this section, we compare the total number of backbone points (S_B , obtained by applying
 396 the backbone extraction algorithm) and the total number of skeleton points (S_s , obtained by
 397 applying the Zhang–Suen image-refinement algorithm) on the same crack segment to measure the
 398 streamlining performance of the crack backbone extraction algorithm proposed in this paper. The
 399 simplification rate of the crack backbone extraction algorithm relative to the Zhang–Suen
 400 image-refinement algorithm is R_e :

$$401 \quad R_e = \frac{S_s - S_B}{S_s} \times 100\% . \quad (14)$$

402 Taking 100 randomly selected crack images as the samples in the experiment, the statistics of
 403 the results obtained are as shown in Fig. 13 and Table 2.



404
405 Fig. 13 Reduction rate test results

406
407 Table 2. Statistical results of the reduction rate test

	Mean	Median	Max	Min	S.D.
Reduction rate	6.40 %	5.82 %	17.04 %	2.60 %	3 %

408

1 409 As shown in Fig. 13 and Table 2, the skeleton obtained by the crack backbone extraction
2 410 algorithm had an average simplification rate of 6.40 % compared with the skeleton obtained using
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4 411 the Zhang–Suen image-refinement algorithm. On the one hand, it showed that the skeleton
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6 412 obtained by the Zhang-Suen image thinning algorithm was universally spaced for further
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8 413 optimization. On the other hand, the measurement direction determination method in this paper
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10 414 was related to the eight-neighborhood pixel distribution of the backbone points, and the
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12 415 streamlining of the skeleton was conducive to the improvement of the matching degree of the
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14 416 macro- and micro-scale measurement direction information of the backbone. Thus, the
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16 417 streamlining performance was good. In addition, it is worth emphasizing that the crack backbone
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18 418 extraction algorithm proposed in this study had no more than two neighboring points for each
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20 419 backbone point, greatly reducing the number of backbone point neighborhood distribution types to
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22 420 only 16, which was convenient for classifying backbone points according to neighborhood
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24 421 distribution types.

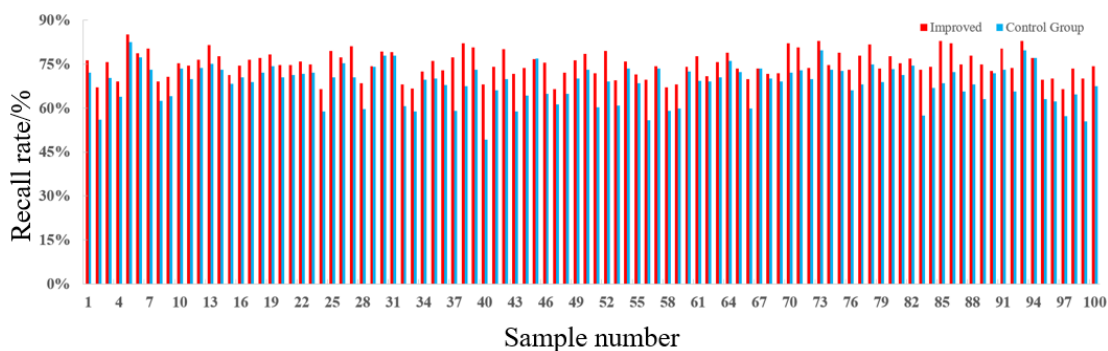
27 422 **3.3 Recall rate of direction determination method**

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31 423 The recall rate of the direction determination method refers to the ratio of the total length of
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33 424 each segment of cracks that can be visually measured in the width to the total length of the cracks
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35 425 in the image, which is used to investigate the recall performance of the measurement algorithm on
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37 426 the task of crack width measurement. On the other hand, the recall rate can also reflect the
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39 427 matching degree between the macro- and micro-scale information of the crack's backbone in the
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41 428 measurement direction determination problem in this method, because the backbone points of the
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43 429 macro- and micro-scale mismatch were the negative sample in the recall statistics. Number of
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45 430 pixels was used to approximate the length of the crack section. Using the direction determination
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47 431 method proposed in this study, the total number of measurable points, P_C , was obtained, and the
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49 432 total number of crack main points, P_S , was counted. The recall rate, R , is given by Eq. (15):

$$51 433 \quad R = \frac{P_C}{P_S} \times 100\% . \quad (15)$$

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53
54 434 In this study, 100 samples were randomly selected on the test set of U-Net crack
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56 435 segmentation, and the segmentation results were used as samples for the recall test. In addition,

436 the control group used the same crack sample set, but the input of direction determination was the
 437 skeleton obtained by the Zhang–Suen thinning algorithm [53]. This was done to demonstrate the
 438 advantages of the proposed backbone extraction algorithm in the direction determination recall.
 439 The recall test results are shown in Fig. 14, where the red label represents the proposed method
 440 and the blue label represents the control group. The statistical results are listed in Table 3, where
 441 the label “Improved” represents the proposed method. The results show that the average recall rate
 442 of the proposed width-measurement direction determination method is approximately 74.90 %, and a
 443 standard deviation of 4 % indicated that the measurement was stable. They all outperformed
 444 the control group; the full-search performance was good overall. At the same time, the results
 445 show that the macro and micro information of the backbone points in the measurement direction
 446 determination problem were well matched, so that averaging three-quarters of the crack sections
 447 can make a more accurate measurement. More accurate here means that measurements with
 448 directions as a guide were theoretically more accurate than the measurement method which did not
 449 distinguish between measurement directions.



451 Fig. 14 Recall rate of the proposed width-measurement direction determination method

452 Table 3 Statistical results of the recall rate of the proposed direction determination method

	Mean	Median	Max	Min	S.D.
Improved	74.90%	74.73%	85.01%	66.36%	4%
Control Group	68.53%	69.82%	82.52%	49.24%	6%

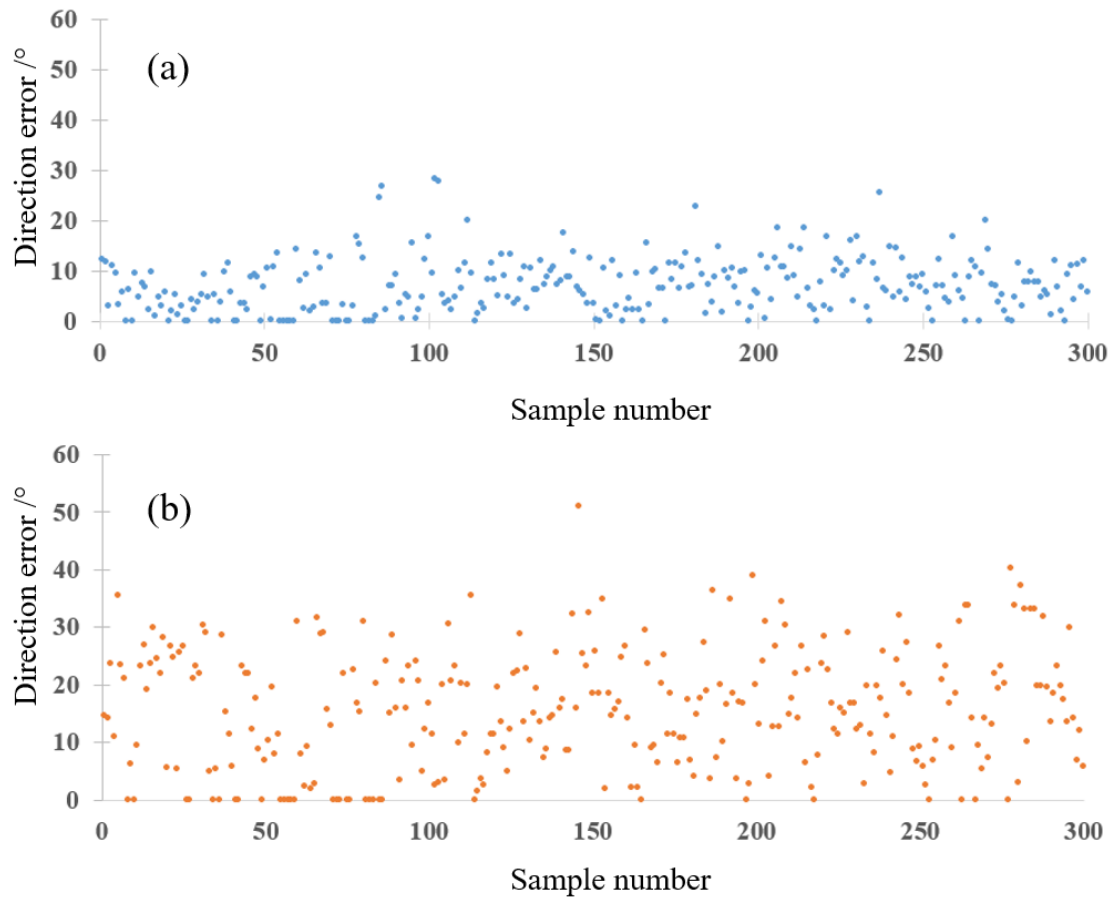
456 3.4 Orientation error of width measurement direction determination

1 457 The direction error was used to evaluate the accuracy of the direction. We randomly selected
2 458 10 backbone points, P_{mi} , from the measurable points, and their positions were recorded and
3
4 459 marked on the image. We invited three technicians to determine the measurement direction of the
5
6 460 crack at the position marked on the image based on their experience, taking the tangential
7
8 461 direction of the crack-growth direction as the measurement direction. Hence, pixel points A and B
9
10 462 were selected on the two edges of the crack, and the mark point, P_m , had to be on the line
11
12 463 section AB or as close to it as possible.

14 464 The width measurement direction determination method was used to determine the
15
16 465 measurement direction of the mark point, P_{mi} , and the crack-edge points, C and D, were recorded
17
18
19 466 in this direction. We composed vectors \overrightarrow{AB} and \overrightarrow{CD} to find the acute angle between them.
20
21 467 $\Delta\theta$ represents the determination error of the measurement direction, as shown in Eq. (16).

$$24 \quad 468 \quad \Delta\theta = \arccos\left(\frac{\overrightarrow{AB} \cdot \overrightarrow{CD}}{|\overrightarrow{AB}| |\overrightarrow{CD}|}\right). \quad (16)$$

27 469 From 30 sample images, 10 points were randomly selected for testing and compared with the
28
29 470 method proposed by Luo et al. [46]. Fig. 15 shows the distribution of the test results.
30
31 471



472
473 Fig. 15. Distribution of direction errors of width measurement direction determination methods: (a)
474 proposed method; (b) method proposed by Luo et al. [46]
475

476 The statistical average, median, maximum, minimum, and standard deviation values are
477 listed in Table 4.
478

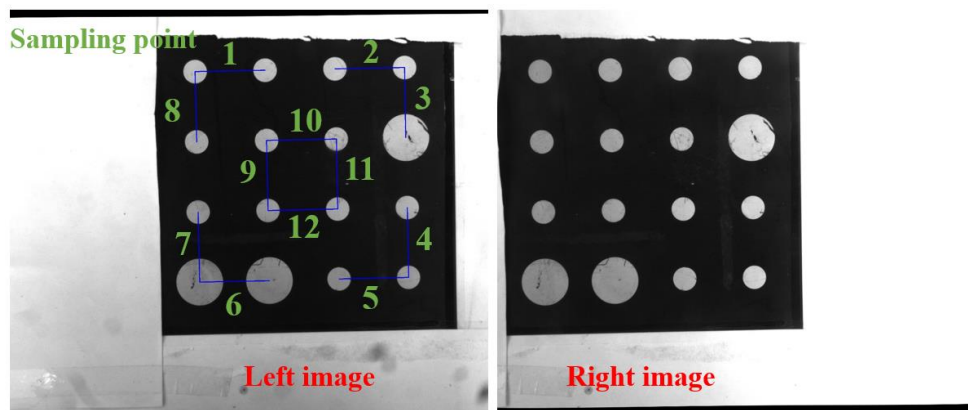
479 Table 4. Direction error statistics of width measurement direction determination methods

	Mean /°	Median /°	Max /°	Mini /°	S.D. /°
Proposed method	6.97	6.45	28.10	0	5.39
Method proposed by Luo et al.[46]	15.44	15.09	51.01	0	10.25

480
481 The direction error of the proposed direction determination method was 6.97°, the median
482 was 6.45°, the standard deviation was 5.39°, and the direction error did not exceed 28.10°, which
483 is significantly better than the method by Luo et al. [46]. The above experiments show that the
484 proposed method to determine the width measurement direction has practical accuracy and
485 stability.

486 **3.5 Test platform accuracy**

487 The spatial distance between the two corner points of the calibration board was calculated by
 488 visual measurement and compared with the actual distance, which can be used to reflect the
 489 measurement accuracy of the test platform in this study. The calibration board was placed on the
 490 dam so that both the left and right cameras could shoot all corners while maintaining the state to
 491 continuously collect 200 images of the calibration board at 2 s intervals, correct them, and select
 492 12 diagonal points on the board as sample points, as shown in Fig. 16.



494 Fig. 16 Left and right images of the calibration board at the test site

497 The error between the visual distance measurement and the actual distance of each sampling
 498 point was used to determine the systematic error of the test device. In the experiment, the average
 499 ($\overline{\mu_B}$) and standard deviation (σ_B) of the error data, maximum absolute error (m_B), average
 500 distance (R_B) from all repeated sampling points to the mean, and distance (D_B) between the
 501 maximum and minimum error data were used to evaluate the test device system error conditions.
 502 The results are presented in Table 5.

504 Table 5. Statistical value of the system error of the test device in this study

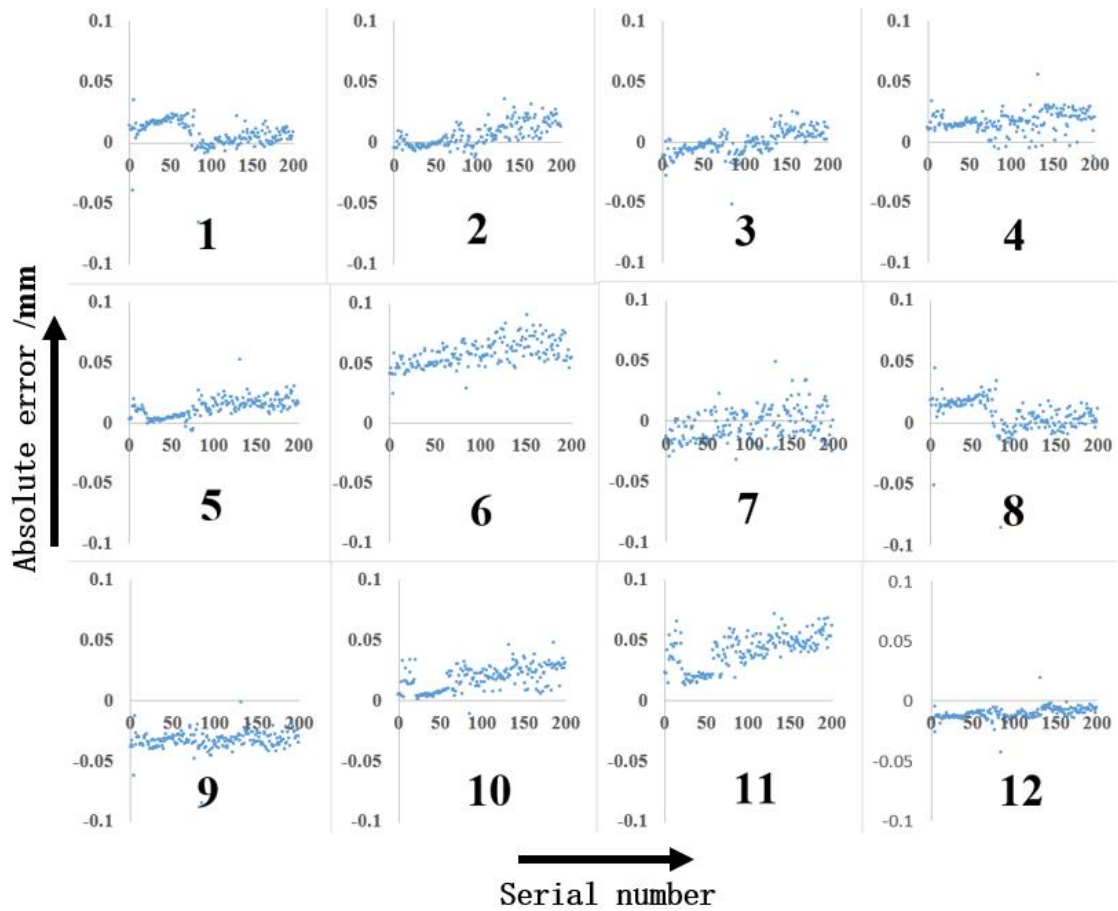
Serial number	$\overline{\mu_B}$	m_B	σ_B	R_B	D_B
Sampling point 1	0.007	0.035	0.011	-0.001	0.101
Sampling point 2	0.006	0.035	0.010	0.006	0.058
Sampling point 3	-0.001	0.024	0.010	-0.001	0.076

Sampling point 4	0.016	0.055	0.009	0.016	0.067
Sampling point 5	0.016	0.052	0.008	0.012	0.059
Sampling point 6	0.058	0.112	0.011	0.057	0.088
Sampling point 7	-0.004	0.0489	0.013	-0.004	0.082
Sampling point 8	0.006	0.044	0.013	-0.013	0.130
Sampling point 9	-0.033	-0.002	0.007	-0.033	0.083
Sampling point 10	0.018	0.048	0.010	0.018	0.059
Sampling point 11	0.040	0.071	0.014	0.040	0.059
Sampling point 12	-0.011	0.019	0.005	-0.011	0.062

505

506 The test results show that in the system error of the test device, $\overline{\mu_B}$, was basically zero,
 507 m_B did not exceed 0.12 mm, σ_B did not exceed 0.014 mm, R_B did not exceed 0.057 mm,
 508 and D_B did not exceed 0.13 mm. Thus, the test device had high accuracy and precision.

509 Fig. 17 shows the distribution of the error data. The horizontal axis represents the sampling
 510 sequence, and the vertical axis represents the measurement error in millimeters.



511

512

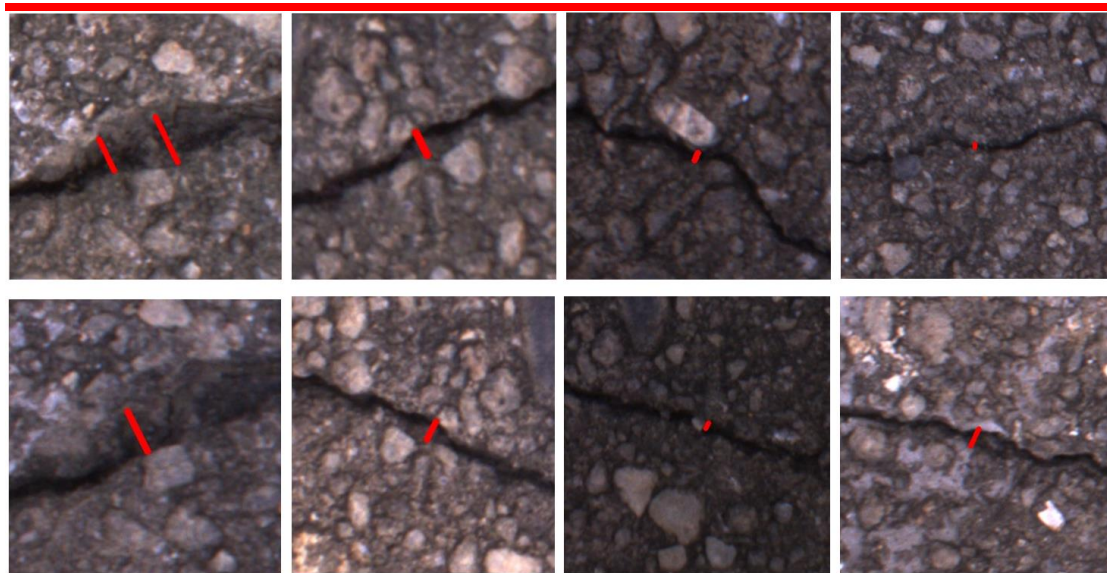
Fig. 17 Error distribution of repeated measurement sampling

513

514 3.6 Field width measurement test

515 The frame of the visual measurement test platform was constructed using aluminum profiles.
516 The main equipment included two MV-EM510C industrial cameras (resolution $2,456 \times 2,058$), the
517 focal length of the lens was 8 mm, and the distance between the camera lens and the dam surface
518 was approximately 240 mm. When installed, the visual axis was perpendicular to the surface of
519 the dam. A digital vernier caliper with an accuracy of 0.01 mm was used to measure the crack
520 width on site for comparison data. The proposed algorithm for determining the measurement
521 direction was used to obtain the measurable points in the crack. Then, five of the measurable
522 points were randomly selected for width measurement, and the measurement position was marked
523 in the real-time image of the left camera. Subsequently, the digital display vernier caliper was used
524 to measure the inner diameter of the crack to obtain the standard value of its width at that location,
525 as shown in Fig 18. The visual measurement value was used for comparison with the standard
526 value. Referring to the experiments in previous studies [26,43,45], the absolute error was used to
527 measure the accuracy of the proposed measurement method.

528



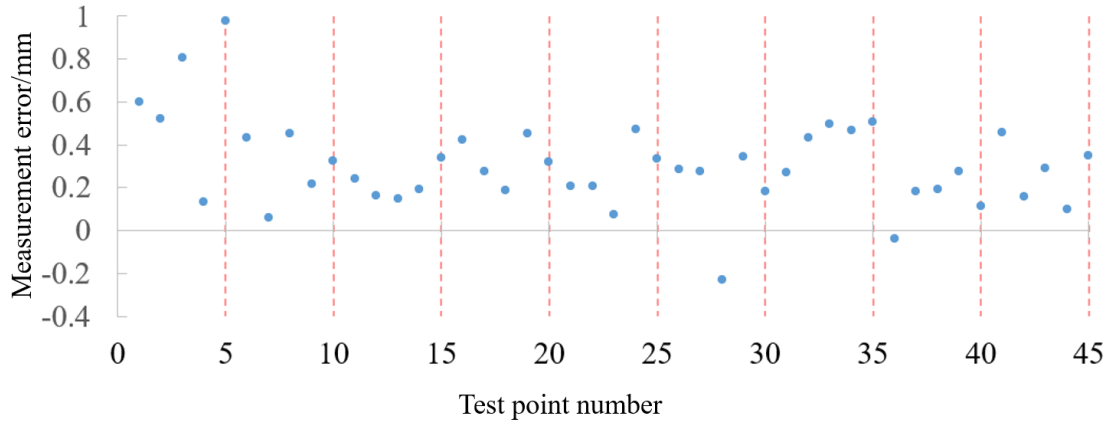
529

530

Fig. 18 Field measurement test

531

532 A total of nine groups were measured in this experiment. The deviation between the width
 533 value measured by the visual measurement and the standard value measured by the digital vernier
 534 caliper is shown in Fig. 19. The average absolute error, $\bar{\mu}$, and the standard deviation, σ , of the
 535 absolute error of each group of data are shown in Table 6.



537 Fig. 19 Deviation of the width value of the visual measurement from the standard value

539 Table 6. Width measurement error average and standard deviation

Group	Error/(mm)	$\bar{\mu}$ /(mm)	σ /(mm)	Group	Error/(mm)	$\bar{\mu}$ /(mm)	σ /(mm)
1	0.60	0.61	0.32	6	0.28	0.26	0.06
	0.52				0.28		
	0.81				-0.23		
	0.13				0.35		
	0.98				0.18		
2	0.43	0.30	0.16	7	0.27	0.43	0.10
	0.06				0.43		
	0.45				0.50		
	0.22				0.47		
	0.33				0.51		
3	0.24	0.22	0.09	8	-0.04	0.16	0.09

	0.16				0.18			
	0.15				0.19			
	0.19				0.28			
	0.34				0.11			
	0.42				0.46			
	0.28				0.16			
4	0.19	0.33	0.11	9	0.29	0.27	0.14	
	0.45				0.10			
	0.32				0.35			
	0.21							
	0.21				$\bar{\mu}$ mean = 0.32 mm			
5	0.07	0.26	0.15					
	0.47							
	0.34				σ mean = 0.19 mm			

541

542 In Fig. 19 and Table 6, the results show that the average error of this test was approximately
543 0.32 mm, and the average variance was 0.19 mm. This demonstrates that the visual measurement
544 test results in this study are close to those of commonly used methods in engineering, which
545 indicates that the proposed method can be utilized in engineering applications.

546

547 **4 Conclusion**

548 This study proposed a practical and complete visual method for measuring crack width using
549 a real dam as the research object. The effectiveness of U-Net in the task of crack segmentation
550 was first verified. Then, to address the problem of data redundancy in the crack skeleton, this
551 study designed a more streamlined and stable crack backbone extraction method. The total number
552 of eight-neighborhood points of each point on the backbone did not exceed two, which reduced
553 the amount of backbone data and the distribution types of the eight neighborhoods of backbone

1 554 points. The backbone's ability to describe the shape of cracks was also enhanced. Furthermore, we
2 555 designed a more accurate method for determining the direction of the crack width measurement by
3
4 556 combining the slope characteristics at the backbone macroscale feature and the neighborhood
5
6 557 distribution characteristics at the microscale feature. We further defined the crack width visual
7
8 558 measurement method according to the measurement direction.
9





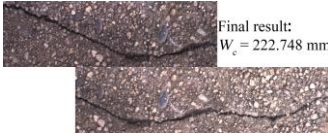
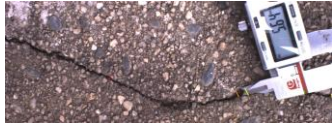
10 559 To evaluate the advantages and disadvantages of the measurement methods, two criteria (i.e.,
11
12 560 recall rate of measurement direction and direction error) were added to provide a technical
13
14 561 reference for subsequent research. Then, we conducted a series of experiments to verify that the
15
16 562 proposed crack backbone extraction algorithm has a good streamlining effect compared to the
17
18 563 Zhang–Suen image-refinement algorithm. Compared with the method presented by Luo et al. [46],
19
20 564 we demonstrated that our proposed method obtains a more accurate width measurement direction.
21
22 565 From the width measurement test, we also demonstrated that it has prospects for practical
23
24 566 engineering applications, and the intelligent degree of structural health monitoring and repair was
25
26 567 improved. The proposed method also provides a reference for the radial vision measurements of
27
28 568 other slender and irregular targets.
29
30

31 569 In the future, for structural damage (e.g., cracks), research on faster, lighter, more accurate,
32
33 570 and more stable image segmentation methods based on U-Net is needed. The visual measurement
34
35 571 process should also be streamlined on the basis of the existing framework to improve the
36
37 572 efficiency of the algorithm. Finally, the three-dimensional reconstruction of cracks should be
38
39 573 explored to improve measurement accuracy and depth measurements so that vision systems will
40
41 574 inherit more comprehensive crack-damage detection capabilities.
42
43
44 575

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46
47
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54
55

56 582 **Appendix A. Examples of processing procedures**

Process	Result	Process	Result
Original		Binarized by U-Net	
Backbone refinement		Curve fitting in Macro scale	
Distance to measuring surface	 Final result: $W_e = 222.748 \text{ mm}$	Width measurement	
P1(783, 1023)	Measurement point 1: (788,1013); Measurement point 2: (778,1033);	Measurement direction: 67.5° Width = 1.936 mm	
P2(1742, 1143)	Measurement point 1: (1731,1121); Measurement point 2: (1749,1158);	Measurement direction: 112.5° Width = 3.563 mm	
P3(1808, 1119)	Measurement point 1: (1796,1095); Measurement point 2: (1822,1148);	Measurement direction: 112.5° Width = 5.112 mm	
P4(2242, 1126)	Measurement point 1: (2242,1117); Measurement point 2: (2242,1140);	Measurement direction: 90° Width = 1.992 mm	
P5(2446, 1147)	Measurement point 1: (2446,1138); Measurement point 2: (2446,1156);	Measurement direction: 90° Width = 1.559 mm	

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Author statement

Yunchao Tang: Conceptualization, Methodology, Writing.

Zhaofeng Huang: Software, Validation.

Zheng Chen: Supervision, Editing.

Minyou Chen: Investigation, Reviewing.

Hao Zhou: Software, Editing.

Hexin Zhang: Editing, Validation.

Junbo Zhang: Data curation.

Editor and Reviewer comments: A major technical revision is needed. Should the authors decide to submit a revised manuscript, they should carefully and thoroughly address all comments offered by the reviewers, and reflect them in the revised manuscript. A point by point response must also be provided with the manuscript.

Reviewer #1:

This research studies the crack width measurement based on machine-vision systems. A backbone refinement algorithm and width-measurement scheme are proposed in this work. The research topic is interesting and within the scope of the Journal. However, from the perspective of the reviewer, the innovation of the proposed approach is not outstanding, and the current manuscript cannot be recommended for publication until the following concerns are carefully addressed.

1. The match of macroscale and microscale information in crack width measurements is significant. Without the match, the proposed methods may appear to be abandoned. Therefore, could you please discuss how to guarantee this match between the microscale and macroscale within your proposed framework?

Thanks for your valuable comments. Revised as suggested.

In this method, there are multiple neighborhood distribution types corresponding to one direction in the microscopic scale information, which is equivalent to adding microscale constraints to the macroscale information, thereby reducing the probability of incorrectly judging the crack width and improving the reliability of the measurement. In fact, using only the macro- or micro-scale information of the backbone for direction judgment may cause a large direction judgment error. Macroscale information is obtained using n-degree polynomials for curve fitting, and the result is a smooth curve, while the crack backbone in the natural state is not a smooth curve, as shown in the newly added Fig.7. On the other hand, at the microscopic scale, only three pixels are used as the basis for directional judgment, which is also not enough to accurately express the growth state of the crack at that place. Therefore, the design method of this paper uses the two-scale information fusion as the basis for judging the measurement direction. The supplement has been added in lines 275-293.

2. The U-Net is an existing method for crack recognition. The innovation of the whole framework is not outstanding. The advantages of the proposed approach should be demonstrated more clearly.

Thanks for your valuable comments. Revised as suggested.

U-Net was originally proposed to deal with the problem of image segmentation of retinal nerves with slender shapes, which has significance for the segmentation of cracks with equally elongated shape features. Previous researchers have used U-Net to study cracks and made progress in stages. By comparing other popular neural networks, this paper demonstrates that U-Net has the advantages of high accuracy and high stability compared with the neural networks used for comparison in crack detection, and has more application prospects. The focus of this article is on the visual measurement of cracks. More introductions to U-Net are supplemented on lines 122 to 129.

3. The figures are recommended to be modified in a more understandable manner. For the bar charts, e.g., Figure 14, the legends are expected to be added.

Thanks for your valuable comments. Revised as suggested.

Figures 4, 6, 7, 8, 9, and 14 have been modified and supplemented.

4. The difference between the proposed crack backbone extraction algorithm should be more clearly clarified in reference to other existing algorithms. In section 3.2, when evaluating the performance of the crack backbone extraction algorithm, please demonstrate the reason for the comparison of the simplification rate, why these indexes are important, and this improvement is significant.

Thanks for your valuable comments. Revised as suggested.

The biggest difference between the crack backbone in this paper and the skeleton extracted by other algorithms is that the crack backbone does not contain small branches, which can be used to express the fracture growth characteristics with more severe cracking. This is because, compared to the small crack branches, the crack backbone with a larger degree of cracking is more worthy of attention. Secondly, only the main crack was considered to make the extracted crack backbone more convenient to serve the width visual measurement, while avoiding the situation that the measurement direction is not unique in the same location. Simplifying the backbone to a single pixel structure is also an element of this research. The simplification rate can be quantified to show that it is meaningful to further study the crack backbone refinement from the general refinement algorithm. This is because after the refinement algorithm, on average, 6.4% of the pixels can still be refined further. The difference between the proposed crack backbone extraction algorithm and other existing algorithms has been added in line 155-158 and line 212-223. A description of the simplification rate has been supplemented in lines 407-416.

5. The recall rate in table reaches nearly 75%, which means the failure rate is still quite high. The samples in subsequent analyses are mentioned to be sampled randomly, but the corresponding results are no distinguished failure cases. Could you please explain the reason why there is no failure cases?

Thanks for your valuable comments. Revised as suggested.

Recall refers to the proportion of pixels on the backbone that can be used to judge the measurement direction. Recall statistics were based on pixels and were used to express the proportion of cracks that can be measured in the entire section, rather than the proportion of crack samples that were not successfully measured to the total sample. The remaining average 25% of the failure cases abandoned the measurement due to a mismatch between the two-scale features. Because the wrong measurement direction did not lead to the correct measurement results, abandoning these positions increased the credibility of the measurement results. Random sampling was done at a measurable location. The procedure did not contain points where the direction of the measurement could not be judged. The purpose of random sampling for measurement was to compare the error between the visual measurement and the actual manual measurement, and the identity case in this section was counted by the measurement direction error and the numerical error of the measurement result. Supplemented on lines 421-424 and 433-444.

6. Finally, the manuscript needs thorough proof reading by a native speaker.

Thanks for your valuable comments. Revised as suggested.

Reviewer #2: In the opinion of the reviewer, this paper is not appropriate for Engineering Structures. Indeed, a detailed description of the way of measuring the crack width is presented, without any correlation with the structural behavior of concrete elements.

Dear reviewer, thanks for your concern. We submitted this paper to the Special Issue "Machine Learning in Structural Engineering". And it fits one of the major interests.

Reviewer #3: This article describes an automated process for determining the width of cracks on the surface of concrete components. The process employs aspects of image analysis and machine learning. The work described by the authors appears to be scientifically sound and it has the potential to be useful to structural engineers who need to assess the cracking characteristics of existing concrete structures.

I recommend that the authors revise the manuscript to address the following concerns:

1. The authors should make the article more accessible to structural engineers who are not familiar with machine learning and image analysis, but who might want to apply the knowledge presented in the article. At a minimum, important technical terms that would not be known by most structural engineers should be defined. For example, it is not clear from the article what exactly is the difference between the "backbone" and the "skeleton". These and other terms need to be explicitly defined.

Thanks for your valuable comments. Revised as suggested.

The meanings of morphological processing, blurring, backbone and skeleton have been supplemented in lines 133-141, 155-158 and 214-225.

Among them, morphological processing here refers to dilation or erosion algorithms (they had opposite effects to each other), whose role is to expand the binarized target towards the background. The role of blur is also to expand the target, but its effect is more moderate than that of morphological processing.

2. The U-Net convolutional network is a key component of the process proposed by the article. Although the authors have correctly given the reference to the article by Ronneberger et al., I believe that U-Net will be unfamiliar to most structural engineers. I recommend that the authors include a brief description of the main features of this network.

Thanks for your valuable comments. Revised as suggested.

U-Net is a semantic segmentation network with 9 levels, which encodes and decodes images. The structure of the encoding stage and the decoding stage are symmetrical, and the shape is named U-shaped. The input of U-Net was an RGB image, and the output is a semantically segmented binary image in this article. The process of semantic segmentation takes place in a code-decoded symmetrical U-shaped structural model, hence the named U-Net. The acquisition of the parameters in the U-shaped structural model requires convolutional inference of a large number of labeled samples, which is then recorded in the model file. When used, the model file is called and the image data is passed into it. The segmentation result can be obtained after calculation by U-Net, which is a very simple and commonly used semantic segmentation model. Related introductions have been added in lines 123-129.

3. The authors consider both a macro-scale and a micro-scale basis for determining the slope of the "backbone" and hence the direction for determining crack width. They should provide a clear explanation of why both scales need to be considered. The significance of the macro-scale basis is fairly clear, given their approach to fitting a polynomial to the backbone and computing its first derivative. The significance of the micro-scale basis is, however, not obvious. In addition, the authors state that then the macro-scale and micro-scale produce different values for the angles ϕ and ψ , then measurement at the given point is abandoned. The authors should explain what this situation corresponds to in physical

terms, perhaps giving some examples of real images.

Thanks for your valuable comments. Revised as suggested.

Macroscopic scale information is obtained using n-degree polynomials for curve fitting, and the result was a smooth curve, while the crack backbone in the natural state was not a smooth curve, as shown in the newly added Fig.7. On the other hand, at the microscopic scale, only three pixels are used as the basis for directional judgment, which was also not enough to accurately express the growth state of the crack at that place. Therefore, the design method of this paper used the two-scale information fusion as the basis for judging the measurement direction. In this method, there were multiple neighborhood distribution types corresponding to one direction in the microscopic scale information, which was equivalent to adding microscale constraints to the macroscale information, thereby reducing the probability of incorrectly judging the crack width and improving the reliability of the measurement. In the blue circle of Fig. 7, manual measurement should be carried out in the 45° direction. However, as shown in the red circle, if microscale information has been used for the measurement, it was measured in the vertical direction. Similarly, in the green circle, the vertical direction should be followed for the manual measurement. However, as shown in the yellow circle, if macroscale information has been used to measure, it was still measured in the 45° direction. In fact, using only the macroscopic or microscopic scale information of the backbone for direction judgment may cause a large direction judgment error. The supplement has been added in lines 204-210, 243-252 and 275-293.

4. The article is not clear on whether the process determines crack width at as many points as possible along the "backbone" or only at points determined by human intervention. This needs to be clarified.





Thanks for your valuable comments. Revised as suggested.

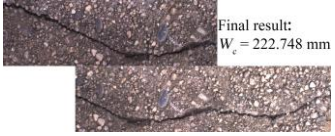
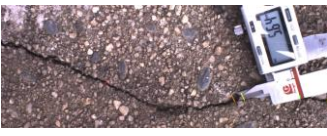
This article is to measure the crack width at as many points as possible along the backbone. The process of determining points with human intervention was just part of the experiment and was used to compare the differences between algorithmic measurements and manual measurements. In practice, all points on the crack where width measurements can be taken should be treated. Supplemented on lines 236-239.

5. It would be helpful for the authors to include, perhaps in conjunction with the flowchart given in Figure 1, an example of how the process they describe actually works, using real images and real numbers. This could perhaps be put into an appendix.

Thanks for your valuable comments. Revised as suggested.

Appendices have been added. For details, please refer to the appendix chapter at the end of the article. Appendix A. Examples of processing procedures

Process	Result	Process	Result
Original		Binarized by U-Net	
Backbone refination		Curve fitting in Macro scale	

Distance to measuring surface	 Final result: $W_c = 222.748 \text{ mm}$	Width measurement	
P1(783, 1023)	Measurement point 1: (788,1013); Measurement point 2: (778,1033);	Measurement direction: 67.5° Width = 1.936 mm	
P2(1742, 1143)	Measurement point 1: (1731,1121); Measurement point 2: (1749,1158);	Measurement direction: 112.5° Width = 3.563 mm	
P3(1808, 1119)	Measurement point 1: (1796,1095); Measurement point 2: (1822,1148);	Measurement direction: 112.5° Width = 5.112 mm	
P4(2242, 1126)	Measurement point 1: (2242,1117); Measurement point 2: (2242,1140);	Measurement direction: 90° Width = 1.992 mm	
P5(2446, 1147)	Measurement point 1: (2446,1138); Measurement point 2: (2446,1156);	Measurement direction: 90° Width = 1.559 mm	

6. The article makes reference to the Zhang-Suen image-refinement algorithm, yet it is not clear what exactly is the difference between the "backbone" extraction algorithm described by the authors and the Zhang-Suen algorithm. This needs to be clarified.

Thanks for your valuable comments. Revised as suggested.

For the convenience of comparison and explanation in the following article, it is stipulated that the output of the Zhang-Suen image thinning algorithm is called "skeleton", and the output proposed for improvement and further processing based on the Zhang-Suen image thinning algorithm in this article is called "backbone". Compared with the classic Zhang-Suen image thinning algorithm, the crack backbone refinement algorithm in this paper has the following characteristics:

1. The effective neighborhood pixels of the backbone are less than 2, and there are only 16 types of neighborhood pixel distribution (as shown in the lower right corner of Fig. 4 and the lower right corner of Fig. 5);
2. The branches were removed and the shape of the end of the crack was retained (as shown in the upper left corner and upper right corner of Fig. 5).

The supplement has been added in lines 155-158 and 214-222.

[Sep. 12, 2022]

[Prof. Yang Jie]
[Editor-in-Chief]
[*ENGINEERING STRUCTURES*]

Dear Editor:

We wish to re-submit an origin article for publication in *Engineering Structures*, entitled “Novel crack-width visual measurement based on backbone double-scale features.”

The manuscript has been rechecked and appropriate changes have been made in accordance with the reviewers’ suggestions. The responses to their comments have been prepared and attached herewith. The manuscript has been proofed by language edit center.

We thank you and the reviewers for your thoughtful suggestions and insights, which have enriched the manuscript and produced a better and more balanced account of the research. We look forward to working with you and the reviewers to move this manuscript closer to publication in *Engineering Structures*.

Thank you for your consideration. We look forward to hearing from you.

Sincerely,
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